



## INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

|   |           |   |
|---|-----------|---|
| (51) International Patent Classification <sup>6</sup> :<br><b>G01N 21/35, G01J 3/42</b>   | <b>A1</b> | (11) International Publication Number: <b>WO 97/21091</b><br>(43) International Publication Date: <b>12 June 1997 (12.06.97)</b>  |
| (21) International Application Number: <b>PCT/AU96/00776</b><br>(22) International Filing Date: <b>2 December 1996 (02.12.96)</b><br>(30) Priority Data:<br><b>PN 6928</b> <b>1 December 1995 (01.12.95)</b> <b>AU</b><br>(71) Applicant (for all designated States except US): <b>COMMON-WEALTH SCIENTIFIC AND INDUSTRIAL RESEARCH ORGANISATION [AU/AU]; Limestone Avenue, Campbell, ACT 2612 (AU).</b><br>(72) Inventors; and<br>(75) Inventors/Applicants (for US only): <b>BAKER, Suzanne, Kay [AU/AU]; 5 Hamer Avenue, Wembley Downs, W.A. 6019 (AU). HENRY, David, Andrew [AU/AU]; 213A Roberts Street, Joondana, W.A. 6060 (AU). PURSER, Douglas, Barrie [AU/AU]; 5 Hamer Avenue, Wembley Downs, W.A. 6019 (AU). DYNES, Robyn, Ann [AU/AU]; 54 Nanson Street, Wembley, W.A. 6014 (AU). WALLINGTON, Brett, Steven [AU/AU]; 51 Magnolia Gardens, Yangebup, W.A. 6164 (AU).</b><br>(74) Agents: <b>HARWOOD, Errol, John et al.; Wray &amp; Associates, 239 Adelaide Terrace, Perth, W.A. 6000 (AU).</b> |           | (81) Designated States: <b>AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, CA, CH, CN, CU, CZ, DE, DK, EE, ES, FI, GB, GE, HU, IL, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MD, MG, MK, MN, MW, MX, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, TJ, TM, TR, TT, UA, UG, US, UZ, VN, ARIPO patent (KE, LS, MW, SD, SZ, UG), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG).</b><br><br><b>Published</b><br><i>With international search report.</i> |
| (54) Title: <b>METHOD FOR DETERMINING FEED QUALITY</b><br>(57) Abstract<br><p>A method for determining a biomechanical property of a feed, the method comprising the steps of: (a) subjecting the feed to infrared radiation to obtain spectral data; and (b) using the spectral data to determine the biomechanical property; whereby, the biomechanical property of the feed is determined on the basis of the bond energies of the chemical constituents of the feed.</p>  |           |   |

**FOR THE PURPOSES OF INFORMATION ONLY**

Codes used to identify States party to the PCT on the front pages of pamphlets publishing international applications under the PCT.

|    |                          |    |  |    |                          |
|----|--------------------------|----|--|----|--------------------------|
| AM | Armenia                  | GB | United Kingdom                           | MW | Malawi                   |
| AT | Austria                  | GE | Georgia                                  | MX | Mexico                   |
| AU | Australia                | GN | Guinea                                   | NE | Niger                    |
| BB | Barbados                 | GR | Greece                                   | NL | Netherlands              |
| BE | Belgium                  | HU | Hungary                                  | NO | Norway                   |
| BF | Burkina Faso             | IE | Ireland                                  | NZ | New Zealand              |
| BG | Bulgaria                 | IT | Italy                                    | PL | Poland                   |
| BJ | Benin                    | JP | Japan                                    | PT | Portugal                 |
| BR | Brazil                   | KE | Kenya                                    | RO | Romania                  |
| BY | Belarus                  | KG | Kyrgyzstan                               | RU | Russian Federation       |
| CA | Canada                   | KP | Democratic People's Republic<br>of Korea | SD | Sudan                    |
| CF | Central African Republic | KR | Republic of Korea                        | SE | Sweden                   |
| CG | Congo                    | KZ | Kazakhstan                               | SG | Singapore                |
| CH | Switzerland              | LI | Liechtenstein                            | SI | Slovenia                 |
| CI | Côte d'Ivoire            | LK | Sri Lanka                                | SK | Slovakia                 |
| CM | Cameroon                 | LR | Liberia                                  | SN | Senegal                  |
| CN | China                    | LT | Lithuania                                | SZ | Swaziland                |
| CS | Czechoslovakia           | LU | Luxembourg                               | TD | Chad                     |
| CZ | Czech Republic           | LV | Latvia                                   | TG | Togo                     |
| DE | Germany                  | MC | Monaco                                   | TJ | Tajikistan               |
| DK | Denmark                  | MD | Republic of Moldova                      | TT | Trinidad and Tobago      |
| EE | Estonia                  | MG | Madagascar                               | UA | Ukraine                  |
| ES | Spain                    | ML | Mali                                     | UG | Uganda                   |
| FI | Finland                  | MN | Mongolia                                 | US | United States of America |
| FR | France                   | MR | Mauritania                               | UZ | Uzbekistan               |
| GA | Gabon                    |    |  | VN | Viet Nam                 |

## Method for Determining Feed Quality

This invention relates to a method for quantifying biomechanical properties of animal feed based on a correlation between the chemical and biomechanical properties of the feed, and to methods for objectively measuring the quality of animal feed, such as fodders including hay, pastures and forages.

Diet is the major determinant of productivity of an animal. In the livestock industry, animals are farmed for meat, wool and other valuable products. The diet of farmed livestock is largely dictated by man and, given the effect of diet on animal production, it is highly desirable to optimise the diet of livestock to gain maximum benefit from the natural resource.

Feed quality is one variable that has a major impact on animal productivity. In this respect, feed quality affects the amount of feed an animal will consume and the feeding value it gains from the feed consumed. In the case of cattle, sheep and other ruminants, feed quality depends on digestibility, chemical attributes (nutrient composition) and biomechanical attributes (namely how easy it is for an animal to chew the feed during ingestion and rumination).

It is generally accepted that there are constraints on the intake of feed by ruminant animals, that the amount of useful energy obtained by a ruminant animal may fall short of the amount that the animal can potentially use, and that this would result in reduced productivity. For example, the principal constraints to voluntary intake of fodders are resistance of fodder fibre to chewing and digestibility (provided that the intake is not otherwise constrained by low palatability, deleterious secondary compounds, or the inadequacy of essential nutrients). Differences between feeds, such as fodders, in their resistance to chewing are reflected in differences in biomechanical properties, including comminution energy, shear energy, compression energy, tensile strength, shear strength and intrinsic shear strength.

Hay is a common feed, and its quality is significantly affected by factors such as seasonal differences, haymaking practices and pasture composition. It has been shown in one recent survey that in some years as little as 11% of hay produced was good enough to promote liveweight gain in weaner sheep. This possibility of wide variation in measures of hay quality is a matter of increasing concern, and has given rise to a demand for a method of objective quality assessment.

A hay quality system adopted in the United States of America uses a measure known as relative feed value (RFV) to distinguish between hays of different quality. The RFV is calculated from the dry matter digestibility, which is predicted from acid detergent fibre (ADF) content, and from the dry matter intake, which is predicted from neutral detergent fibre (NDF) content.

The RFV based system suffers from a number of disadvantages. For example, the ADF and NDF contents of fodders are determined by chemical methods which take several days to complete, and thus are expensive in terms of resources.

While objective quality assessment and product specification has become an integral part of the production and marketing in domestic and export markets for the Australian grain, wool, meat and dairy industries, performance-based quality standards are not presently in place for feeds such as hays and other fodders. Consequently;

(a) the feed buyer cannot be sure of getting value for money, and this is likely to become increasingly important in respect of export markets if other exporting countries are able to guarantee standards for their product;

(b) the feed producer cannot be sure of getting a higher price for a superior product;

- (c) livestock producers are unable to objectively formulate rations or supplementary feeding regimes to achieve animal production targets; and
  - (d) the market for animal feed tends to be unstable.
- 5 Whilst the relationship between biomechanical properties of feed and feed quality is now accepted, there is a need for a convenient, inexpensive and relatively accurate assay method for feed to determine its quality. An accurate determination of feed quality allows for optimisation of feeding regimes and improved animal production for obvious economic gains.
- 10 It is an object of this invention to overcome or at least partially alleviate the aforementioned problems and/or reduce the uncertainties and concomitant problems of the prior art systems for measuring the biomechanical properties of feed and hence determining feed quality.

Thus, the present invention provides a method for determining a biomechanical  
15 property of a feed, the method comprising the steps of;

- (a) subjecting the feed to infrared radiation to obtain spectral data; and
- (b) using the spectral data to determine the biomechanical property;

whereby the biomechanical property of the feed is determined on the basis of  
20 the bond energies of the chemical constituents of the feed.

The spectral data may be used directly to determine the biomechanical property of the feed. Alternatively, the spectral data may be used to determine another property of the feed and the other property is used to determine the biomechanical property on the basis of a correlation between the other property  
25 and the biomechanical property.

When the biomechanical property is determined via another property, the other property is preferably a chemical property of the feed such as the ADF content or the NDF content or the lignin content.

5 There is a variety of biomechanical properties of the feed that may be determined. Preferably, the biomechanical properties are selected from the group comprising shear energy, compression energy, comminution energy, tensile strength, shear strength and intrinsic shear strength.

10 The spectral data may comprise a reflectance spectrum at a combination of wavelengths or over a predetermined range of wavelengths such as 700nm-3000nm, or more preferably 1100nm-2500nm. Preferably, the data obtained for the spectral range of 1850nm-1970nm is disregarded, this being the range over which water reflects strongly.

15 The spectral data may be recorded at one or more wavelength intervals throughout the spectral range. When the spectral data is a reflectance spectrum over a predetermined range it is preferably measured at 2nm intervals over the range. Of course, if so desired the spectral data may be measured at intervals other than 2nm.

20 When the spectral data is used to directly determine a biomechanical property, the biomechanical property is preferably determined by comparison of the spectral data with a calibration equation that reflects the relationship between reflectance and the biomechanical property. Preferably, the calibration curve is determined on the basis of laboratory data establishing a correlation between reflectance and the biomechanical property.

25 Thus, the present invention also provides a method for determining a biomechanical property of a feed, the method comprising the steps of;

- (a) subjecting the feed to infrared radiation to obtain spectral data;
- and

- (b) comparing the spectral data obtained in (a) with a calibration equation to determine the biomechanical property;

whereby the biomechanical property of the feed is determined on the basis of the bond energies of the chemical constituents of the feed.

- 5 The present invention also provides a method for determining feed quality, the method comprising the steps of;

- (a) subjecting the feed to infrared radiation to obtain spectral data;
- (b) using the spectral data to determine a biomechanical property of the feed; and
- 10 (c) using the value of the biomechanical property obtained in step (b) to determine feed quality;

---

whereby the biomechanical property of the feed and thus the feed quality is determined on the basis of the bond energies of the chemical constituents of the feed.

- 15 In one particular form, the method described immediately above may further comprise the determination of an additional property of the feed. The additional property may vary and preferably is selected from the group comprising the digestibility of the feed *in vivo* or *in vitro*, the ADF content or the NDF content, or the lignin content.
  - 20 The present invention is based on research establishing a strong correlation between the bond energies as they relate to the physical structure, and the biomechanical properties of feed. Once this correlation is established the bond energies of the chemical constituents, and in turn the biomechanical properties of the feed, can be determined using infrared spectroscopy. The biomechanical
-

properties quantified in this way are useful for accurately determining feed quality.

In this respect, research resulting in the present invention has shown that the biomechanical attributes of feeds such as cereal and legume hays, straws, and  
5 mature, dry subterranean clovers are much more strongly related to animal performance than are digestibility or chemical composition of the feeds.

Thus, comminution energy, the energy required to grind or comminute fodder material, has proved to be a very effective indicator of forage consumption constraint (FCC), which is the difference between the quantity of forage an  
10 animal should consume to satisfy its capacity to use energy (a theoretical maximum) and the actual voluntary dry matter intake achieved.

Shear energy, the energy required to shear fodder material, and compression energy, the energy required to compress fodder material, are two biomechanical  
feed characters of fodders that are closely related to comminution energy and  
15 which also are good predictors of FCC.

In this respect, feed quality can be assessed in a number of ways. The forage consumption constraint (FCC) is one convenient measure of feed quality and equates to the difference between the quantity of the fodder that the animal would be attempting to consume to satisfy its capacity to use energy (theoretical  
20 maximum intake) and the voluntary forage consumption (VFC).

Thus, the present invention also provides a method for determining feed quality, the method comprising the steps of;

- (a) subjecting the feed to infrared radiation to obtain spectral data;
- (b) using the spectral data to determine a biomechanical property of  
25 the feed; and



- (c) using the value of the biomechanical property obtained in step (b) to determine the forage consumption constraint (FCC) or voluntary feed consumption (VFC) as a measure of feed quality;

whereby the biomechanical property of the feed and thus the feed quality is  
5 determined on the basis of the bond energies of the chemical constituents of the feed.

The present invention is based on the finding that variations in biomechanical properties such as shear energy, comminution energy and compression energy are reflected in NIR spectra of fodders. This finding, together with recognition of  
10 the value of biomechanical characters for the prediction of FCC (and, in turn, the prediction of voluntary feed consumption (VFC) ) makes it possible for quicker, less expensive, more convenient and more reliable prediction of feed quality than hitherto known and predicted.

Accordingly, this invention provides a method of (i) assessing the suitability of a  
15 fodder, such as a forage, to meet a required animal performance; or (ii) predicting the VFC of a forage; or (iii) predicting the FCC of a forage, which method comprises subjecting a sample of the forage to NIR radiation and determining the reflectance at selected wavelengths.

It has been found that the biomechanical properties, such as shear and  
20 comminution energy values for a given fodder, correlate with the fodder's reflectance of infrared radiation. More specifically, the invention is based on research showing that:

- (a) NIR wavelengths at which reflectance (R), namely the second derivative of the logarithm of the inverse of R, correlates significantly with the variation in  
25 energy required to shear fodder materials are 1168nm, 1458nm, 1598nm, 1718nm, 1828nm and 2048nm. For the prediction of fodder shear energy ( $y_1$ ,  $\text{kJ.m}^{-2}$ ) the following equation may be used:

$$y_1 = 19.95 + 10239.46 R_{1168} + 3623.49 R_{1458} - 4255.61 R_{1598} - 5319.88 R_{1718} + 5148.38 R_{1828} + 2452.05 R_{2048}$$

- (b) NIR wavelengths at which the second derivative of the logarithm of the inverse of reflectance (R) correlates significantly with the variation in energy required to comminute fodder materials are 1138nm, 2018nm, 2128nm and 2408nm.

For the prediction of fodder comminute energy ( $y_2$ , kJ.kg DM<sup>-1</sup>) the following equation is proposed:

$$y_2 = 231.42 + 18224.74 R_{1138} - 4955.12 R_{2018} - 3005.37 R_{2128} + 4290.18 R_{2408}$$

- (c) NIR wavelengths at which the second derivative of the logarithm of the inverse of reflectance (R) correlates significantly with the variation in compression energy are 1268nm, 1588nm, 1728nm, 2278nm. For the prediction of compression energy ( $y_3$ , kJ.kgDM<sup>-1</sup>) the following equation may be used:

$$y_3 = -0.71 - 911.04 R_{1268} + 112.57 R_{1588} - 79.48 R_{1728} - 28.02 R_{2278}$$

- (d) NIR wavelengths at which the second derivative of the logarithm of the inverse of reflectance (R) correlates significantly with variation in *in vivo* digestibility of dry matter (DMD) ( $y_4$ , %) is 1158nm, 1238nm, 1668nm, 1908nm, 1918nm, and 2248nm. For prediction of the DMD ( $y_4$ , %) of a fodder the following equation is proposed:

$$y_4 = 46.62 + 8162.72 R_{1158} - 8799.69 R_{1238} + 1249.01 R_{1668} + 519.46 R_{1908} - 367.08 R_{1918} - 161.84 R_{2248}$$

- (e) NIR wavelength at which the second derivative of the logarithm of the inverse of reflectance (R) correlates significantly with variation in *in vitro*

digestibility of dry matter (IVDMD) is 1698nm, 1748nm, 1908nm, 1918nm and 2158nm. For prediction of the DMD (*in vitro*) of a fodder the following equation is proposed:

$$y_5 = 63.43 - 2186.89 R_{1698} - 1491.99 R_{1748} + 981.30 R_{1908} - 556.01 R_{1918} + 2003.05 R_{2158}$$

Accordingly, in a preferred method according to this invention, the infrared wavelengths at which reflectance is measured comprise one or more of the following: 1168nm, 1458nm, 1598nm, 1718nm, 1828nm, 2048nm, 1138nm, 2018nm, 2128nm, 2408nm, 1268nm, 1588nm, 1728nm, 2278nm, 1158nm, 1238nm, 1668nm, 1908nm, 2248nm, 1698nm, 1748nm, 1918nm and 2158nm.

It will be understood that the foregoing are wavelengths at which the strongest correlations have been observed, and the possibility of useful correlations being observed at other wavelengths are highly likely.

Essentially, it can be shown that in the same way that a decrease in comminution energy is reflected by a decrease in forage consumption constraint, there is also a linear relationship between comminution energy or shear energy and the consumption constraint of a fodder. Thus, the use of NIR spectra, in conjunction with the equations detailed at paragraphs (a) to (e) above, permits estimation of the VFC of a fodder, which together with estimates of digestibility (conveniently obtained from NIR spectra) can be expected to provide a valuable basis for performance-based quality standards for fodders.

It is to be appreciated that the intention of this invention is to offer a quick, reliable and relatively inexpensive means of obtaining information from which the fodder producer and user, such as purchaser, might make informed judgements about the market value of a given fodder sample relative to alternatives, and of its suitability for a particular purpose.

Conceivably, fodder quality predictions obtained by the method of this invention could be a useful component of, or used in conjunction with, for example, Decision Support Software (DSS) packages designed to assist livestock management.

- 5 It is further envisaged that by combining NIR measurements made by a remote sensing system, such as Landsat, with data from a Geographical Information System, the invention will provide a means of making reliable predictions of pasture quality. These predictions, together with predictions of feed intake and animal performance, should then provide a useful basis  
10 for strategies of supplementary feeding to improve performance in grazing ruminants.

- The present invention also provides for a spectrometer configured to determine biomechanical properties and/or quality of feed according to the methods of the present invention. Preferably, the spectrometer includes a  
15 data processing means which enables the spectrometer to receive a feed sample and quantify either or both the biomechanical properties of the feed and the quality of the feed. In one particular form the data processing means includes a calibration equation to facilitate the determination of the feed quality or biomechanical property.

- 20 The invention will now be described with reference to the following examples. The description of the examples is in no way to limit the generality of the preceding paragraphs.

### EXAMPLES

The energy of molecular vibrations correspond to the energy of the infrared spectrum of the electromagnetic spectrum, and these molecular vibrations may be detected and measured in the wavelength range of the infrared spectrum.

- 5 Functional groups in molecules have vibration frequencies that are characteristic of that functional group and that are within well-defined regions of the infrared spectrum.

- For organic compounds the principal analytical features of the near infrared (NIR) spectrum are due to absorbance of radiant energy by bonds between hydrogen, carbon, nitrogen, oxygen or with sulphur, phosphorus and metal halides. When organic compounds are irradiated with infrared radiation at wavelengths between 700 and 3000nm part of the incident radiation is absorbed and the remainder is reflected, refracted or transmitted by the sample. Most
- 10 quantitative reflectance analyses are made in the wavelength range of 1100 to 2600nm. The amount of energy absorbed or diffusely reflected at any given wavelength in this wavelength range is related to the chemical composition of the organic compound. NIR spectroscopy uses detectors to measure the amount of radiation that is diffusely reflected by the irradiated sample.

20

- NIR spectroscopic analysis is an analytical procedure calibrated to a primary reference method. Calibration in NIR spectroscopy (NIRS) relies on similarities among the spectra, and analytical properties of interest in the reference samples. In this example the analytical properties of interest were the
- 25 biomechanical characters of forages, and the procedure that was adopted in this example was as follows:

- a) prediction of biomechanical characters of a range of grasses using NIR spectroscopy was established by developing a calibration equation(s) from
- 30 laboratory determined values of a set of reference samples.

- b) validation of the equation(s) either by using laboratory determined values of a separate set of samples, or by a cross-validation procedure using the laboratory determined values of the reference samples.
  - c) using the NIRS-predicted values for biomechanical characters of the forages and for digestibility of the forages, forage consumption constraint (FCC) was predicted, and in turn voluntary feed consumption (VFC) was predicted.
  - d) the predicted FCC and VFC were compared with actual data from groups of animals fed each of these forages.
- 10 Example A: Developing a calibration equation to predict biomechanical properties of herbage:
- The samples used in this example were a range of varieties of *Panicum spp.* harvested at a range of plant maturities throughout the growing season (Table
- 15 1). Each of the samples was dried and chaffed, and then fed to groups of sheep (8 sheep per group) which were penned individually, to determine *in vivo* dry matter digestibility (DMD), VFC and FCC. Samples of the hays were stored for laboratory analyses.
- 20 Biomechanical properties of the forages were determined using published methods; the energies required to shear or compress the forages according to Baker, Klein, de Boer and Purser (Genotypes of dry, mature subterranean clover differ in shear energy. Proceedings of the XVII International Grassland Congress 1993. pp 592-593.) and the energy required to comminute the forages
- 25 according to Weston and Davis (The significance of four forage characters as constraints to voluntary intake. Proceedings of the Third International Symposium on the Nutrition of Herbivores, Penang, 1991). *In vitro* digestibility of dry matter (IVDMD) was determined by the pepsin-cellulase technique as modified by Klein and Baker (Composition of the fractions of dry, mature
- 30 subterranean clover digested *in vivo* and *in vitro*. Proceedings of the XVII International Grassland Congress 1993. pp593-595.).

There are several ways to process samples for NIRS analysis, and in this example the samples were ground through a cyclone mill with a 1 mm screen and equilibrated at 25°C for at least 24h before NIRS analysis. The samples were scanned by a monochromating near infrared reflectance spectrophotometer (Perstorp NIRS 6500) and the absorption spectra recorded for the range 1100 to 2500nm at 2nm intervals. The spectral range 1850 to 1970nm, where water absorbs strongly, was disregarded in further analysis of the spectral data.

10 For NIRS analysis the samples were divided into two groups: one group to be used as a 'calibration' set to establish a prediction equation, and a second group, the 'validation' set, to be used to validate the prediction equation. There are a number of ways to select the samples for each set. In this example the samples were ranked according to each of the characters that were to be  
15 predicted and every other sample was selected for the calibration set (33 samples) and the validation set (32 samples). Thus, for each character that was evaluated, a different selection was made from the 65 samples to establish the respective calibration and validation sample sets.

20 The ranges, mean, median and variation in the laboratory-determined values for each of the characters of interest in the calibration and validation sets are listed in Table 2.

The software for scanning, mathematical processing and statistical analysis were  
25 supplied with the spectrophotometer by the manufacturers. The spectral data were transformed by taking the second derivative of the logarithm of the inverse of the reflectance (R) at each wavelength ( $d^2 \log (1/R)$ ). The similarities amongst the spectra (Figure 1) of the samples in the validation and calibration sets were determined using principal components scores to rank the spectra according to  
30 the Mahalanobis distance from the average of the spectra. The Mahalanobis distance values were standardized by dividing them by their average value, and were denoted 'global' H values (Table 3).

Calibration equations were developed using the calibration samples by regressing the data from the laboratory analyses of each biomechanical property against the corresponding transformed spectral data using the following  
5 mathematical methods:

- a) Stepwise linear regression
- b) Step-up linear regression
- c) Principal components regression (PCR)
- 10 d) Partial least squares regression (PLS), and
- e) Modified partial least squares regression (MPLS).

Stepwise calibrations were developed for each calibration set of samples using the mathematical treatments of the spectral data 2,2,2; 2,5,5; 2,10,5; and  
15 2,10,10; where the first number denotes that the second derivative was used, the second indicates that second derivatives of the spectral data (determined at 2nm intervals) were taken at intervals of 4, 10 or 20nm, and the third indicates that the function was smoothed using the 'boxcar' method over intervals of wavelength of 4, 10, or 20nm (Table 4a). Likewise step-up calibrations were  
20 developed for each calibration set with up to 6 terms in each calibration equation using mathematical treatments 2,2,2; 2,5,5; 2,10,5; and 2,10,10 (Table 4b). Calibrations developed for each calibration set using principal components regression, partial least squares regression, or modified partial least squares regression each were developed using mathematical treatments 2,5,5 and  
25 2,10,10 (Table 4c).

In developing the calibration equations in the stepwise and step-up regressions, only wavelengths with partial F-statistic of more than 8 were accepted for the models.

30

For each calibration using each calibration set the following calibration statistics were determined:



- a) Squared multiple correlation coefficient ( $R^2$ ), an indication of the proportion of the variation in the calibration set that is adequately modelled by the calibration equation.
- b) The standard error of calibration (SEC) together with its confidence interval ( $\pm$  CL), which is the standard deviation for the residuals due to difference between the laboratory determined (reference) and the NIR predicted values for samples within the calibration set

Once the calibration equations were developed, each equation was validated by using it to predict the respective biomechanical property values for each sample in the validation sample set. For each calibration equation the following validation statistics were determined:

- a) Simple linear correlation coefficient ( $r^2$ ) between the laboratory determined and NIR predicted values.
- b) The bias (or systematic error) in the regression relationship between the laboratory determined (reference) and NIR predicted values.
- c) The confidence limits of the bias in the regression relationship between the laboratory determined (reference) and NIR predicted values.
- d) The standard error of prediction, corrected for bias (SEP(C)), which represents the unexplained error of the prediction, the deviation of the differences between laboratory determined and NIR predicted values.
- e) The coefficient of determination, or slope ( $\beta$ ), and y-intercept ( $\alpha$ ) of the linear regression relationship between the laboratory determined and NIR predicted values.
- f) The residual standard deviation (RSD) of the linear regression relationship between the laboratory determined and NIR predicted values.

In addition, the calibration equations were validated using a procedures of cross-validation. These are procedures where every sample in the calibration set was used once for prediction, and the standard error of validation corrected for bias (SEV(C), for stepwise and step-up regressions) and cross-validation (SECV, for multivariate regressions) can be determined.

Calibration equations for each biomechanical character were selected using the following criteria:

- a) Lowest partial F-ratio, highest  $R^2$ , lowest SEC and, for PCR, PLS and MPLS, lowest SEV(C) (or, for multivariate regressions, SECV)
- b) Highest  $r^2$ , lowest bias and  $|\text{bias}| < \text{bias confidence limit}$ , lowest SEP(C),  $\beta$  closest to 1.0,  $\alpha$  closest to 0, and lowest RSD. As well, SEP(C) was compared with the standard error of laboratory determined values amongst all 65 samples, listed in Table 5.

Calibration equations were similarly established to predict *in vivo* digestibility and *in vitro* digestibility. The coefficients for each wavelength in the selected calibration equations from stepwise or step-up regression analyses are listed in Table 6a, and those from multivariate analyses are listed in Table 6b.

Simple linear correlation coefficient ( $r^2$ ) between the laboratory determined and NIR predicted values for each of the biomechanical characters (energies required to shear, comminute or compress) and digestibility of dry matter determined *in vivo* or *in vitro* of the samples in the validation set are shown in Figures 2a, 2b, and 2c. The NIR predicted values are predicted using calibration equations that best met the criteria listed above.

Example B: Prediction of FCC and VFC using NIR determinations of energy required to shear and *in vivo* digestibility:

To demonstrate the prediction of voluntary feed consumption using NIR determined values for a biomechanical character and digestibility of forages, samples of *Panicum spp.* hay were selected which were common to both of the validation sample sets used to establish the NIR prediction equations for energy required to shear and *in vivo* digestibility. The hays represented the range of varieties in the sample set, and are listed in Table 7. The samples were scanned by the same spectrophotometer that was used to establish the

calibration equations, and the absorption spectra were recorded in the range 1100 to 2500nm at 2nm intervals. Values for energy required to shear and *in vivo* digestibility were predicted from calibration equations (Tables 4a, 4b and 4c) using the recorded spectral data.

5

These values then were used to estimate FCC from the relationship between biomechanical character(s) and FCC of the range of forages used by Weston and Davis (1991). Energy required to shear the forages used by Weston and Davis was determined according to Baker *et al.* (1993). The relationship  
10 between the energy required to shear these forages ( $\text{kJ/m}^2$ ) and FCC (g organic matter (OM) / d / kg metabolic body weight (MBW)) was described by the relationship:

$$\text{Energy required to shear (x)} = -26.13 + 5.53 (\text{FCC (y)})$$

where  $R = 0.92$ ;  $\text{RSD} = 8.70$ ;  $N = 13$ ;  $P < 0.0001$ .

15

FCC from this relationship and *in vivo* digestibility predicted by NIR were then used to estimate VFC, as the difference between the animal's capacity to use energy (as defined by Weston and Davis, 1991) and FCC. These data are summarised in Table 8.

20

VFC predicted in this way explained most of the variation in actual VFC ( $R = 0.87$ ;  $\text{RSD} = 5.04$ ;  $P = 0.023$ ) (Figure 3).

Table 1. Description of herbage used in this example.

| Genus          | Species               | Variety              | Common name      | Part of plant | Process undergone | Stage of maturity                | Regrowth               |
|----------------|-----------------------|----------------------|------------------|---------------|-------------------|----------------------------------|------------------------|
| <i>Panicum</i> | <i>coloratum</i>      | Bambatal             | Makarikeri grass | serial        | dried and chaffed | late bloom (9 weeks' regrowth)   | late bloom - regrowth  |
| <i>Panicum</i> | <i>coloratum</i>      | Bambatal             | Makarikeri grass | serial        | dried and chaffed | late bloom (13 weeks' regrowth)  | late bloom - regrowth  |
| <i>Panicum</i> | <i>coloratum</i>      | Bambatal             | Makarikeri grass | serial        | dried and chaffed | late bloom (4 weeks' regrowth)   | late bloom - regrowth  |
| <i>Panicum</i> | <i>coloratum</i>      | Bambatal             | Makarikeri grass | serial        | dried and chaffed | mid bloom (1 month's regrowth)   | mid bloom - regrowth   |
| <i>Panicum</i> | <i>coloratum</i>      | Bambatal             | Makarikeri grass | serial        | dried and chaffed | mid bloom (1 month's regrowth)   | mid bloom - regrowth   |
| <i>Panicum</i> | <i>coloratum</i>      | Bambatal             | Makarikeri grass | serial        | dried and chaffed | mid bloom (10 weeks' regrowth)   | mid bloom - regrowth   |
| <i>Panicum</i> | <i>coloratum</i>      | Bambatal             | Makarikeri grass | serial        | dried and chaffed | mid bloom (8 weeks' regrowth)    | mid bloom - regrowth   |
| <i>Panicum</i> | <i>coloratum</i>      | Bambatal             | Makarikeri grass | serial        | dried and chaffed | vegetative regrowth (29 days)    | vegetative regrowth    |
| <i>Panicum</i> | <i>coloratum</i>      | Kabulabula CPI 18798 | Makarikeri grass | serial        | dried and chaffed | late bloom                       | late bloom             |
| <i>Panicum</i> | <i>coloratum</i>      | Kabulabula CPI 18798 | Makarikeri grass | serial        | dried and chaffed | late bloom (4 weeks' regrowth)   | late bloom - regrowth  |
| <i>Panicum</i> | <i>coloratum</i>      | Kabulabula CPI 18798 | Makarikeri grass | serial        | dried and chaffed | late bloom (19 weeks' regrowth)  | late bloom - regrowth  |
| <i>Panicum</i> | <i>coloratum</i>      | Kabulabula CPI 18798 | Makarikeri grass | serial        | dried and chaffed | late bloom (14 weeks' regrowth)  | late bloom - regrowth  |
| <i>Panicum</i> | <i>coloratum</i>      | Kabulabula CPI 18798 | Makarikeri grass | serial        | dried and chaffed | mid bloom (8 weeks' regrowth)    | mid bloom - regrowth   |
| <i>Panicum</i> | <i>coloratum</i>      | Kabulabula CPI 18798 | Makarikeri grass | serial        | dried and chaffed | mid bloom (8 weeks' regrowth)    | mid bloom - regrowth   |
| <i>Panicum</i> | <i>coloratum</i>      | Kabulabula CPI 18798 | Makarikeri grass | serial        | dried and chaffed | vegetative regrowth (28 days)    | vegetative regrowth    |
| <i>Panicum</i> | <i>coloratum</i>      | Burnett              | Makarikeri grass | serial        | dried and chaffed | early bloom (1 month's regrowth) | early bloom - regrowth |
| <i>Panicum</i> | <i>Makarikeriense</i> | Burnett              | Makarikeri grass | serial        | dried and chaffed | late bloom (14 weeks' regrowth)  | late bloom - regrowth  |
| <i>Panicum</i> | <i>coloratum</i> var  | Burnett              | Makarikeri grass | serial        | dried and chaffed | late bloom (4 weeks' regrowth)   | late bloom - regrowth  |
| <i>Panicum</i> | <i>Makarikeriense</i> | Burnett              | Makarikeri grass | serial        | dried and chaffed | mid bloom (8 weeks' regrowth)    | mid bloom - regrowth   |
| <i>Panicum</i> | <i>coloratum</i> var  | Burnett              | Makarikeri grass | serial        | dried and chaffed | mid bloom (10 weeks' regrowth)   | mid bloom - regrowth   |
| <i>Panicum</i> | <i>Makarikeriense</i> | Burnett              | Makarikeri grass | serial        | dried and chaffed | vegetative regrowth (31 days)    | vegetative regrowth    |
| <i>Panicum</i> | <i>coloratum</i> var  | Burnett              | Makarikeri grass | serial        | dried and chaffed | mid bloom (1 month's regrowth)   | mid bloom - regrowth   |
| <i>Panicum</i> | <i>Makarikeriense</i> | Burnett              | Makarikeri grass | serial        | dried and chaffed | mid bloom (4 weeks' regrowth)    | mid bloom - regrowth   |
| <i>Panicum</i> | <i>coloratum</i> var  | Burnett              | Makarikeri grass | serial        | dried and chaffed | late bloom (4 weeks' regrowth)   | late bloom - regrowth  |
| <i>Panicum</i> | <i>Makarikeriense</i> | Burnett              | Makarikeri grass | serial        | dried and chaffed | mid bloom (13 weeks' regrowth)   | mid bloom - regrowth   |
| <i>Panicum</i> | <i>coloratum</i> var  | Burnett              | Makarikeri grass | serial        | dried and chaffed | mid bloom (10 weeks' regrowth)   | mid bloom - regrowth   |
| <i>Panicum</i> | <i>maximum</i>        | Colonio              | Guinea grass     | serial        | dried and chaffed |                                  |                        |
| <i>Panicum</i> | <i>maximum</i>        | Colonio              | Guinea grass     | serial        | dried and chaffed |                                  |                        |
| <i>Panicum</i> | <i>maximum</i>        | Colonio              | Guinea grass     | serial        | dried and chaffed |                                  |                        |

Table 1. Description of herbage used in this example.

(cont'd)

| Genus   | Species | Variety | Common name  | Part of plant | Process undergone | Stage of maturity                | Regrowth               |
|---------|---------|---------|--------------|---------------|-------------------|----------------------------------|------------------------|
| Panicum | maximum | Colonio | Guinea grass | seral         | dried and chaffed | vegetative regrowth (4 weeks')   | vegetative regrowth    |
| Panicum | maximum | Colonio | Guinea grass | seral         | dried and chaffed | vegetative regrowth (33 days')   | vegetative regrowth    |
| Panicum | maximum | Colonio | Guinea grass | seral         | dried and chaffed | vegetative regrowth (28 days')   | vegetative regrowth    |
| Panicum | maximum | Colonio | Guinea grass | seral         | dried and chaffed | vegetative regrowth (1 month's)  | vegetative regrowth    |
| Panicum | maximum | Colonio | Guinea grass | seral         | dried and chaffed | vegetative regrowth (1 month's)  | vegetative regrowth    |
| Panicum | maximum | Colonio | Guinea grass | seral         | dried and chaffed | vegetative regrowth (8 weeks')   | vegetative regrowth    |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | early bloom (1 month's regrowth) | early bloom - regrowth |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | early bloom (10 weeks' regrowth) | early bloom - regrowth |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | late bloom (4 weeks' regrowth)   | late bloom - regrowth  |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | late bloom (13 weeks' regrowth)  | late bloom - regrowth  |
| Panicum | maximum | Hamill  | Guinea grass | leaf          | dried and chaffed | 54 days' regrowth                | regrowth               |
| Panicum | maximum | Hamill  | Guinea grass | leaf          | dried and chaffed | 75 days' regrowth                | regrowth               |
| Panicum | maximum | Hamill  | Guinea grass | leaf          | dried and chaffed | 88 days' regrowth                | regrowth               |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | vegetative (8 weeks' regrowth)   | vegetative             |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | vegetative regrowth (8 weeks')   | vegetative regrowth    |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | vegetative regrowth (32 days')   | vegetative regrowth    |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | late bloom (8 weeks' regrowth)   | late bloom - regrowth  |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | late bloom (1 month's regrowth)  | late bloom - regrowth  |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | mid bloom (10 weeks' regrowth)   | mid bloom - regrowth   |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | mid bloom (14 weeks' regrowth)   | mid bloom - regrowth   |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | mid bloom (15 weeks' regrowth)   | mid bloom - regrowth   |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | mid bloom (15 weeks' regrowth)   | mid bloom - regrowth   |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | mid bloom (8 weeks' regrowth)    | mid bloom - regrowth   |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | mid bloom (1 month's)            | mid bloom - regrowth   |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | mid bloom (13 weeks' regrowth)   | mid bloom - regrowth   |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | mid bloom (4 weeks' regrowth)    | mid bloom - regrowth   |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | mid bloom (11 weeks' regrowth)   | mid bloom - regrowth   |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | vegetative regrowth (28 days')   | vegetative regrowth    |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | vegetative regrowth (32 days')   | vegetative regrowth    |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | vegetative regrowth (4 weeks')   | vegetative regrowth    |
| Panicum | maximum | Hamill  | Guinea grass | seral         | dried and chaffed | vegetative regrowth (4 weeks')   | vegetative regrowth    |

Table 2. Summary statistics for each calibration and validation set

|   | Energy required<br>to shear<br>(kJ/m <sup>2</sup> ) | Energy required<br>to comminute<br>(kJ/kg DM) | Energy required<br>to compress<br>(kJ/kg DM) | Digestibility of<br>dry matter <i>in vivo</i><br>(%) | Digestibility of dry<br>matter <i>in vitro</i><br>(%) |
|---|---|---|--|--|---|
| <b>Energy required to shear</b>                   |   |   |  |  |   |
| <b>Calibration set</b>                            |   |   |  |  |   |
| mean  | 15.48   | 134.9   | 3.70   | 55.7   | 53.3  |
| median  | 15.17   | 133.8   | 3.65   | 56.0   | 55.1  |
| maximum   | 20.95   | 216.5   | 4.39   | 64.0   | 63.0  |
| minimum   | 10.80   | 72.5  | 3.25   | 43.0   | 39.8  |
| standard deviation                                | 2.572   | 37.50   | 0.265  | 5.73   | 6.97  |
| <b>Validation set</b>                             |   |   |  |  |   |
| mean  | 15.43   | 130.9   | 3.78   | 55.6   | 52.7  |
| median  | 15.20   | 128.3   | 3.75   | 56.5   | 53.3  |
| maximum   | 20.43   | 205.2   | 4.24   | 64.0   | 63.0  |
| minimum   | 10.94   | 54.5  | 3.34   | 47.0   | 40.1  |
| standard deviation                                | 2.444   | 37.50   | 0.229  | 5.36   | 7.01  |
| <b>Energy required to comminute</b>               |   |   |  |  |   |
| <b>Calibration set</b>                            |   |   |  |  |   |
| mean  | 15.01   | 133.1   | 3.69   | 55.7   | 52.8  |
| median  | 14.76   | 129.5   | 3.70   | 57.0   | 54.7  |
| maximum   | 19.97   | 216.5   | 4.18   | 64.0   | 63.0  |
| minimum   | 10.80   | 54.5  | 3.25   | 43.0   | 39.8  |
| standard deviation                                | 2.444   | 38.82   | 0.227  | 5.64   | 7.06  |
| <b>Validation set</b>                             |   |   |  |  |   |
| mean  | 15.92   | 132.9   | 3.79   | 55.6   | 53.2  |
| median  | 15.97   | 130.2   | 3.79   | 55.5   | 54.7  |
| maximum   | 20.95   | 205.2   | 4.39   | 64.0   | 62.5  |
| minimum   | 11.46   | 60.7  | 3.34   | 47.0   | 40.9  |
| standard deviation                                | 2.490   | 36.20   | 0.263  | 5.47   | 6.92  |
| <b>Energy required to compress</b>                |   |   |  |  |   |
| <b>Calibration set</b>                            |   |   |  |  |   |
| mean  | 15.28   | 128.1   | 3.74   | 56.3   | 53.8  |
| median  | 15.07   | 128.4   | 3.72   | 57.0   | 54.7  |
| maximum   | 19.97   | 204.0   | 4.39   | 64.0   | 63.0  |
| minimum   | 10.80   | 54.5  | 3.25   | 47.0   | 39.8  |
| standard deviation                                | 2.477   | 38.00   | 0.261  | 5.15   | 6.64  |
| <b>Validation set</b>                             |   |   |  |  |   |
| mean  | 15.64   | 138.0   | 3.74   | 55.0   | 52.2  |
| median  | 15.42   | 132.5   | 3.72   | 54.5   | 54.5  |
| maximum   | 20.95   | 216.5   | 4.24   | 64.0   | 62.0  |
| minimum   | 11.46   | 60.7  | 3.34   | 43.0   | 40.1  |
| standard deviation                                | 2.530   | 36.39   | 0.240  | 5.87   | 7.26  |
| <b>Digestibility of dry matter <i>in vivo</i></b> |   |   |  |  |   |
| <b>Calibration set</b>                            |   |   |  |  |   |
| mean  | 15.14   | 133.9   | 3.74   | 55.5   | 53.1  |
| median  | 15.17   | 128.4   | 3.72   | 56.0   | 55.1  |
| maximum   | 20.95   | 216.5   | 4.24   | 64.0   | 63.0  |
| minimum   | 10.80   | 60.7  | 3.25   | 43.0   | 40.1  |
| standard deviation                                | 2.528   | 36.39   | 0.247  | 5.73   | 7.33  |
| <b>Validation set</b>                             |   |   |  |  |   |
| mean  | 15.78   | 132.1   | 3.75   | 55.7   | 52.9  |
| median  | 15.20   | 134.7   | 3.72   | 56.5   | 54.4  |
| maximum   | 20.37   | 205.2   | 4.39   | 64.0   | 63.0  |
| minimum   | 10.94   | 54.5  | 3.34   | 47.0   | 39.8  |
| standard deviation                                | 2.446   | 38.70   | 0.255  | 5.36   | 6.63  |

RECTIFIED SHEET (RULE 91)

Table 2 (cont'd). Summary statistics for each calibration and validation set

|  | Energy required to shear<br>(kJ/m <sup>2</sup> ) | Energy required to comminute<br>(kJ/kg DM) | Energy required to compress<br>(kJ/kg DM) | Digestibility of dry matter <i>in vivo</i><br>(%) | Digestibility of dry matter <i>in vitro</i><br>(%) |
|--|--|--|---|---|--|
| <b>Digestibility of dry matter <i>in vitro</i></b> |  |  |   |   |  |
| <b>Calibration set</b>                             |  |  |   |   |  |
| mean   | 14.70  | 131.3                                      | 3.75                                      | 55.6  | 53.0   |
| median   | 14.34  | 129.3                                      | 3.71                                      | 56.0  | 54.7   |
| maximum  | 19.36  | 216.5                                      | 4.39                                      | 64.0  | 63.0   |
| minimum  | 10.80  | 54.5                                       | 3.25                                      | 43.0  | 40.1   |
| standard deviation                                 | 2.235  | 42.58                                      | 0.241                                     | 5.78  | 6.94   |
| <b>Validation set</b>                              |  |  |   |   |  |
| mean   | 16.19  | 134.6                                      | 3.74                                      | 55.6  | 53.0   |
| median   | 16.16  | 133.8                                      | 3.74                                      | 56.0  | 54.7   |
| maximum  | 20.95  | 194.8                                      | 4.24                                      | 64.0  | 63.0   |
| minimum  | 10.94  | 65.7                                       | 3.34                                      | 47.0  | 39.8   |
| standard deviation                                 | 2.538  | 31.84                                      | 0.260                                     | 5.33  | 7.05   |

Table 3. Mahalanobis distances

|   | Mean  | Median | Range         |
|---|-------|--------|---------------|
| For full sample set:                        | 0.655 | 0.623  | 0.203 - 1.983 |
| For calibration sets for:                   |       |        |               |
| Energy required to shear                    | 0.588 | 0.549  | 0.171 - 1.646 |
| Energy required to comminute                | 0.718 | 0.676  | 0.350 - 1.553 |
| Energy required to compress                 | 0.757 | 0.760  | 0.188 - 1.440 |
| Digestibility of dry matter <i>in vivo</i>  | 0.673 | 0.634  | 0.389 - 1.547 |
| Digestibility of dry matter <i>in vitro</i> | 0.645 | 0.574  | 0.185 - 1.178 |

Table 4a. Calibration and validation statistics

| Energy required to shear     |                     |         |         |         |
|------------------------------|---------------------|---------|---------|---------|
|                              | Stepwise Regression |         |         |         |
|                              | 2,2,2               | 2,5,5   | 2,10,5  | 2,10,10 |
| Lowest partial F-ratio       | 10.27               | 6.18    | 8.27    | 4.70    |
| R <sup>2</sup>               | 0.798               | 0.787   | 0.795   | 0.780   |
| SEC                          | 1.155               | 1.188   | 1.166   | 1.207   |
| SEC CL                       | 1.493               | 1.535   | 1.507   | 1.560   |
| SEV(C)                       | 1.230               | 1.306   | 1.273   | 1.322   |
| r <sup>2</sup>               | 0.368               | 0.625   | 0.520   | 0.495   |
| Bias                         | 0.690               | 0.710   | 0.700   | 0.720   |
| Bias CL                      | 1.484               | 1.527   | 1.498   | 1.551   |
| SEP (C)                      | 1.500               | 1.540   | 1.520   | 1.570   |
| Slope                        | 0.604               | 0.617   | 0.598   | 0.758   |
| Intercept                    | 6.340               | 5.440   | 5.640   | 3.710   |
| R.S.D.                       | 1.627               | 1.627   | 1.484   | 1.476   |
| Bias  - Bias CL              | -0.794              | -0.817  | -0.798  | -0.831  |
| Bias  < Bias CL?             | Yes                 | Yes     | Yes     | Yes     |
| number of terms              | 6                   | 5       | 5       | 6       |
| Energy required to comminute |                     |         |         |         |
|                              | Stepwise Regression |         |         |         |
|                              | 2,2,2               | 2,5,5   | 2,10,5  | 2,10,10 |
| Lowest partial F-ratio       | 5.54                | 4.45    | 16.55   | 10.89   |
| R <sup>2</sup>               | 0.910               | 0.802   | 0.818   | 0.831   |
| SEC                          | 11.626              | 17.281  | 16.546  | 15.980  |
| SEC CL                       | 1.493               | 1.535   | 1.507   | 1.560   |
| SEV(C)                       | 13.103              | 18.040  | 17.587  | 17.100  |
| r <sup>2</sup>               | 0.363               | 0.429   | 0.374   | 0.213   |
| Bias                         | 6.980               | 10.370  | 9.930   | 9.590   |
| Bias CL                      | 14.941              | 22.209  | 21.264  | 20.537  |
| SEP (C)                      | 15.110              | 22.460  | 21.510  | 20.770  |
| Slope                        | 0.530               | 0.575   | 0.607   | 0.417   |
| Intercept                    | 58.300              | 48.900  | 48.600  | 74.600  |
| R.S.D.                       | 28.900              | 27.360  | 28.650  | 32.120  |
| Bias  - Bias CL              | -7.961              | -11.839 | -11.334 | -10.947 |
| Bias  < Bias CL?             | Yes                 | Yes     | Yes     | Yes     |
| number of terms              | 6                   | 3       | 4       | 4       |
| Energy required to compress  |                     |         |         |         |
|                              | Stepwise Regression |         |         |         |
|                              | 2,2,2               | 2,5,5   | 2,10,5  | 2,10,10 |
| Lowest partial F-ratio       | 5.05                | 4.44    | 7.90    | 16.19   |
| R <sup>2</sup>               | 0.784               | 0.500   | 0.525   | 0.534   |
| SEC                          | 0.121               | 0.209   | 0.204   | 0.202   |
| SEC CL                       | 1.493               | 1.535   | 1.507   | 1.560   |
| SEV(C)                       | 0.135               | 0.224   | 0.217   | 0.215   |
| r <sup>2</sup>               | 0.069               | 0.113   | 0.008   | 0.067   |
| Bias                         | 0.070               | 0.130   | 0.120   | 0.120   |
| Bias CL                      | 0.156               | 0.269   | 0.262   | 0.260   |
| SEP (C)                      | 0.160               | 0.270   | 0.270   | 0.260   |
| Slope                        | 0.180               | -0.080  | 0.314   | 0.211   |
| Intercept                    | 3.060               | 4.030   | 2.580   | 2.960   |
| R.S.D.                       | 0.229               | 0.229   | 0.227   | 0.232   |
| Bias  - Bias CL              | -0.086              | -0.139  | -0.142  | -0.140  |
| Bias  < Bias CL?             | Yes                 | Yes     | Yes     | Yes     |
| number of terms              | 6                   | 4       | 4       | 4       |



Table 4a (cont'd)

| Dig stibility of dry matter <i>in vivo</i>  |                     |        |        |         |
|---|---------------------|--------|--------|---------|
|   | Stepwis Regression  |        |        |         |
|   | 2,2,2               | 2,5,5  | 2,10,5 | 2,10,10 |
| Lowest partial F-ratio                      | 7.63                | 20.68  | 4.28   | 6.08    |
| R <sup>2</sup>                              | 0.934               | 0.917  | 0.914  | 0.921   |
| SEC   | 1.107               | 1.236  | 1.258  | 1.207   |
| SEC CL                                      | 1.493               | 1.535  | 1.507  | 1.560   |
| SEV(C)                                      | 1.215               | 1.368  | 1.341  | 1.284   |
| r <sup>2</sup>                              | 0.654               | 0.881  | 0.878  | 0.876   |
| Bias  | 1.070               | 0.890  | 0.910  | 0.900   |
| Bias CL                                     | 0.156               | 0.269  | 0.262  | 0.260   |
| SEP (C)                                     | 2.320               | 1.940  | 1.980  | 1.960   |
| Slope                                       | 0.705               | 0.878  | 0.840  | 0.827   |
| Intercept                                   | 16.500              | 6.690  | 8.640  | 9.340   |
| R.S.D.                                      | 3.153               | 1.852  | 1.873  | 1.888   |
| Bias  - Bias CL                             | 0.914               | 0.621  | 0.648  | 0.640   |
| Bias  < Bias CL?                            | No                  | No     | No     | No      |
| number of terms                             | 6                   | 6      | 6      | 5       |
| Digestibility of dry matter <i>in vitro</i> |                     |        |        |         |
|   | Stepwise Regression |        |        |         |
|   | 2,2,2,1             | 2,5,5  | 2,10,5 | 2,10,10 |
| Lowest partial F-ratio                      | 7.68                | 11.84  | 4.33   | 6.31    |
| R <sup>2</sup>                              | 0.935               | 0.933  | 0.915  | 0.922   |
| SEC   | 1.808               | 1.751  | 2.052  | 1.974   |
| SEC CL                                      | 1.493               | 1.535  | 1.507  | 1.560   |
| SEV(C)                                      | 1.984               | 1.981  | 2.186  | 2.100   |
| r <sup>2</sup>                              | 0.699               | 0.847  | 0.743  | 0.736   |
| Bias  | 1.080               | 1.050  | 1.230  | 1.180   |
| Bias CL                                     | 2.324               | 2.250  | 2.637  | 2.537   |
| SEP (C)                                     | 2.340               | 2.280  | 2.670  | 2.570   |
| Slope                                       | 0.839               | 0.962  | 0.775  | 0.763   |
| Intercept                                   | 8.790               | 1.650  | 12.200 | 12.700  |
| R.S.D.                                      | 3.805               | 3.794  | 3.805  | 2.719   |
| Bias  - Bias CL                             | -1.244              | -1.200 | -1.407 | -1.357  |
| Bias  < Bias CL?                            | Yes                 | Yes    | Yes    | Yes     |
| number of terms                             | 6                   | 5      | 6      | 5       |

Table 4b. Calibration and validation statistics (Step-up regression)

|                              | Energy required to clear |         |         |         |         |         | Step-up Regression 2,2,2 |         |         |         |         |         | Step-up Regression 2,5,5 |         |         |         |         |         |
|------------------------------|--------------------------|---------|---------|---------|---------|---------|--------------------------|---------|---------|---------|---------|---------|--------------------------|---------|---------|---------|---------|---------|
|                              | 1 term                   | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 1 term                   | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 1 term                   | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms |
| Lowest partial F-ratio       | 29.33                    | 13.83   | 6.65    | 5.29    | 5.89    | 3.23    |                          |         |         |         |         |         | 25.70                    | 21.99   | 5.71    | 1.60    | 4.92    | 1.70    |
| R <sup>2</sup>               | 0.470                    | 0.625   | 0.664   | 0.725   | 0.766   | 0.784   |                          |         |         |         |         |         | 0.436                    | 0.663   | 0.709   | 0.715   | 0.778   | 0.792   |
| SEC                          | 1.873                    | 1.575   | 1.445   | 1.349   | 1.244   | 1.196   |                          |         |         |         |         |         | 1.932                    | 1.492   | 1.387   | 1.373   | 1.211   | 1.173   |
| SEC CL                       | 2.420                    | 2.035   | 1.867   | 1.743   | 1.608   | 1.546   |                          |         |         |         |         |         | 2.497                    | 1.928   | 1.792   | 1.774   | 1.565   | 1.516   |
| SEV(C)                       | 1.973                    | 1.672   | 1.561   | 1.476   | 1.390   | 1.318   |                          |         |         |         |         |         | 2.022                    | 1.571   | 1.476   | 1.470   | 1.357   | 1.319   |
| r <sup>2</sup>               | 0.371                    | 0.344   | 0.310   | 0.205   | 0.202   | 0.168   |                          |         |         |         |         |         | 0.375                    | 0.531   | 0.557   | 0.557   | 0.631   | 0.635   |
| Bias                         | 1.120                    | 0.950   | 0.870   | 0.810   | 0.775   | 0.720   |                          |         |         |         |         |         | 1.160                    | 0.900   | 0.830   | 0.820   | 0.730   | 0.700   |
| Bias CL                      | 2.407                    | 2.024   | 1.857   | 1.734   | 1.599   | 1.537   |                          |         |         |         |         |         | 2.483                    | 1.917   | 1.783   | 1.765   | 1.556   | 1.507   |
| SEP (C)                      | 2.430                    | 2.050   | 1.880   | 1.750   | 1.620   | 1.550   |                          |         |         |         |         |         | 2.510                    | 1.940   | 1.800   | 1.780   | 1.570   | 1.520   |
| Slope                        | 1.000                    | 0.795   | 0.784   | 0.598   | 0.549   | 0.498   |                          |         |         |         |         |         | 0.643                    | 0.606   | 0.616   | 0.633   | 0.644   | 0.633   |
| Intercept                    | -0.120                   | 3.030   | 3.290   | 6.090   | 6.950   | 7.790   |                          |         |         |         |         |         | 5.390                    | 5.790   | 5.560   | 5.270   | 5.050   | 5.170   |
| R.S.D.                       | 1.896                    | 1.803   | 1.773   | 1.769   | 1.732   | 2.058   |                          |         |         |         |         |         | 1.891                    | 1.806   | 1.698   | 1.658   | 2.317   | 1.945   |
| Bias  - Bias CL              | -1.287                   | -1.074  | -0.987  | -0.924  | -0.824  | -0.817  |                          |         |         |         |         |         | -1.323                   | -1.017  | -0.953  | -0.945  | -0.826  | -0.807  |
| Bias  < Bias CL?             | Yes                      | Yes     | Yes     | Yes     | Yes     | Yes     |                          |         |         |         |         |         | Yes                      | Yes     | Yes     | Yes     | Yes     | Yes     |
| Energy required to eliminate |                          |         |         |         |         |         |                          |         |         |         |         |         |                          |         |         |         |         |         |
|                              | Step-up Regression 2,2,2 |         |         |         |         |         | Step-up Regression 2,5,5 |         |         |         |         |         | Step-up Regression 2,5,5 |         |         |         |         |         |
|                              | 1 term                   | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 1 term                   | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 1 term                   | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms |
| Lowest partial F-ratio       | 81.33                    | 12.82   | 9.62    | 6.10    | 6.71    | 2.92    |                          |         |         |         |         |         | 67.30                    | 8.96    | 2.73    | 4.91    | 5.06    | 4.26    |
| R <sup>2</sup>               | 0.715                    | 0.794   | 0.840   | 0.864   | 0.887   | 0.894   |                          |         |         |         |         |         | 0.974                    | 0.741   | 0.755   | 0.782   | 0.810   | 0.830   |
| SEC                          | 20.719                   | 17.629  | 15.538  | 14.330  | 13.061  | 12.620  |                          |         |         |         |         |         | 22.149                   | 19.757  | 19.213  | 18.105  | 16.921  | 15.983  |
| SEC CL                       | 2.420                    | 2.035   | 1.867   | 1.743   | 1.608   | 1.546   |                          |         |         |         |         |         | 2.497                    | 1.928   | 1.792   | 1.774   | 1.565   | 1.516   |
| SEV(C)                       | 21.511                   | 18.353  | 16.378  | 15.230  | 13.967  | 13.633  |                          |         |         |         |         |         | 22.769                   | 20.547  | 20.096  | 19.092  | 18.262  | 17.484  |
| r <sup>2</sup>               | 0.322                    | 0.424   | 0.421   | 0.411   | 0.371   | 0.373   |                          |         |         |         |         |         | 0.183                    | 0.199   | 0.148   | 0.099   | 0.114   | 0.098   |
| Bias                         | 12.430                   | 10.580  | 9.320   | 8.600   | 7.840   | 7.570   |                          |         |         |         |         |         | 13.290                   | 11.850  | 11.530  | 10.860  | 10.150  | 9.590   |
| Bias CL                      | 26.627                   | 22.656  | 19.969  | 18.416  | 16.785  | 16.219  |                          |         |         |         |         |         | 28.465                   | 25.391  | 24.692  | 23.268  | 21.746  | 20.541  |
| SEP (C)                      | 26.940                   | 22.920  | 20.200  | 18.630  | 16.980  | 16.410  |                          |         |         |         |         |         | 28.790                   | 25.680  | 24.980  | 23.540  | 22.000  | 20.780  |
| Slope                        | 0.605                    | 0.623   | 0.577   | 0.560   | 0.524   | 0.521   |                          |         |         |         |         |         | 0.491                    | 0.518   | 0.441   | 0.346   | 0.365   | 0.317   |
| Intercept                    | 47.100                   | 43.900  | 48.900  | 52.900  | 58.300  | 57.800  |                          |         |         |         |         |         | 60.100                   | 58.500  | 70.800  | 84.600  | 82.700  | 89.600  |
| R.S.D.                       | 29.810                   | 27.480  | 27.550  | 27.790  | 28.720  | 28.670  |                          |         |         |         |         |         | 32.720                   | 32.400  | 33.420  | 34.370  | 34.070  | 34.380  |
| Bias  - Bias CL              | -14.197                  | -12.076 | -10.649 | -9.816  | -8.945  | -8.649  |                          |         |         |         |         |         | -15.175                  | -13.541 | -13.162 | -12.408 | -11.596 | -10.951 |
| Bias  < Bias CL?             | Yes                      | Yes     | Yes     | Yes     | Yes     | Yes     |                          |         |         |         |         |         | Yes                      | Yes     | Yes     | Yes     | Yes     | Yes     |

Table 4b. (cont'd)

| Energy required to compress                |        |         |         |         |         |         |  |                          |         |         |         |         |         |
|--|--------|---------|---------|---------|---------|---------|--|--------------------------|---------|---------|---------|---------|---------|
| Step-up Regression 2,2,2                   |        |         |         |         |         |         |  | Step-up Regression 2,5,5 |         |         |         |         |         |
|  | 1 term | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms |  | 1 term                   | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms |
| Lowest partial F-ratio                     | 7.28   | 6.24    | 3.22    | 2.65    | 3.10    | 0.00    |  | 8.07                     | 4.23    | 4.08    | 2.21    | 5.36    | 1.87    |
| R <sup>2</sup>                             | 0.164  | 0.285   | 0.334   | 0.370   | 0.440   | 0.530   |  | 0.181                    | 0.258   | 0.327   | 0.445   | 0.520   | 0.535   |
| SEC  | 0.270  | 0.250   | 0.241   | 0.235   | 0.221   | 0.203   |  | 0.268                    | 0.255   | 0.243   | 0.220   | 0.205   | 0.202   |
| SEC CL                                     | 2.420  | 2.035   | 1.867   | 1.743   | 1.608   | 1.546   |  | 2.497                    | 1.928   | 1.792   | 1.774   | 1.565   | 1.516   |
| SEV(C)                                     | 0.277  | 0.259   | 0.252   | 0.248   | 0.238   | 0.226   |  | 0.276                    | 0.268   | 0.257   | 0.241   | 0.227   | 0.222   |
| r <sup>2</sup>                             | 0.067  | 0.089   | 0.087   | 0.104   | 0.067   | 0.033   |  | 0.039                    | 0.064   | 0.038   | 0.005   | 0.010   | 0.006   |
| Bias                                       | 0.160  | 0.150   | 0.140   | 0.140   | 0.130   | 0.120   |  | 0.160                    | 0.150   | 0.150   | 0.130   | 0.120   | 0.120   |
| Bias CL                                    | 0.347  | 0.321   | 0.310   | 0.302   | 0.284   | 0.261   |  | 0.344                    | 0.328   | 0.312   | 0.283   | 0.263   | 0.260   |
| SEP (C)                                    | 0.350  | 0.330   | 0.310   | 0.310   | 0.290   | 0.260   |  | 0.350                    | 0.330   | 0.320   | 0.290   | 0.270   | 0.260   |
| Slope                                      | 0.367  | 0.394   | 0.345   | 0.341   | 0.280   | 0.156   |  | 0.267                    | 0.295   | 0.198   | 0.068   | 0.085   | 0.063   |
| Intercept                                  | 2.380  | 2.270   | 2.460   | 2.470   | 2.690   | 3.160   |  | 2.750                    | 2.640   | 3.010   | 3.490   | 3.420   | 3.510   |
| R.S.D.                                     | 0.235  | 0.232   | 0.235   | 0.239   | 0.239   | 0.239   |  | 0.236                    | 0.233   | 0.230   | 0.229   | 0.233   | 0.239   |
| Bias  - Bias CL                            | -0.187 | -0.171  | -0.170  | -0.162  | -0.154  | -0.141  |  | -0.184                   | -0.178  | -0.162  | -0.153  | -0.143  | -0.140  |
| Bias  < Bias CL?                           | Yes    | Yes     | Yes     | Yes     | Yes     | Yes     |  | Yes                      | Yes     | Yes     | Yes     | Yes     | Yes     |
| Digestibility of dry matter <i>In vivo</i> |        |         |         |         |         |         |  |                          |         |         |         |         |         |
| Step-up Regression 2,2,2                   |        |         |         |         |         |         |  | Step-up Regression 2,5,5 |         |         |         |         |         |
|  | 1 term | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms |  | 1 term                   | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms |
| Lowest partial F-ratio                     | 72.42  | 5.79    | 8.71    | 16.80   | 13.18   | 2.86    |  | 80.75                    | 12.35   | 8.41    | 7.34    | 6.03    | 3.72    |
| R <sup>2</sup>                             | 0.616  | 0.714   | 0.830   | 0.862   | 0.883   | 0.906   |  | 0.679                    | 0.826   | 0.897   | 0.909   | 0.919   | 0.924   |
| SEC  | 3.555  | 3.069   | 2.365   | 2.127   | 1.962   | 1.755   |  | 3.248                    | 2.394   | 1.840   | 1.728   | 1.635   | 1.586   |
| SEC CL                                     | 2.420  | 2.035   | 1.867   | 1.743   | 1.608   | 1.546   |  | 2.497                    | 1.928   | 1.792   | 1.774   | 1.565   | 1.516   |
| SEV(C)                                     | 3.666  | 3.250   | 2.557   | 2.312   | 2.152   | 1.956   |  | 3.328                    | 2.457   | 1.972   | 1.884   | 1.828   | 1.782   |
| r <sup>2</sup>                             | 0.785  | 0.712   | 0.684   | 0.787   | 0.884   | 0.768   |  | 0.755                    | 0.740   | 0.884   | 0.893   | 0.876   | 0.869   |
| Bias                                       | 2.130  | 1.840   | 1.420   | 1.280   | 1.180   | 1.050   |  | 1.950                    | 1.440   | 1.100   | 1.040   | 0.980   | 0.950   |
| Bias CL                                    | 0.347  | 0.321   | 0.310   | 0.302   | 0.284   | 0.261   |  | 0.344                    | 0.328   | 0.312   | 0.283   | 0.263   | 0.260   |
| SEP (C)                                    | 4.620  | 3.990   | 3.070   | 2.770   | 2.550   | 2.280   |  | 4.220                    | 3.110   | 2.390   | 2.250   | 2.130   | 2.060   |
| Slope                                      | 1.050  | 0.805   | 0.792   | 0.826   | 0.777   | 0.731   |  | 1.090                    | 1.050   | 0.889   | 0.880   | 0.866   | 0.885   |
| Intercept                                  | -2.180 | 10.300  | 11.000  | 9.040   | 11.900  | 14.900  |  | -5.290                   | -3.300  | 5.850   | 6.430   | 7.210   | 6.080   |
| R.S.D.                                     | 2.484  | 2.877   | 2.584   | 2.652   | 2.734   | 3.108   |  | 2.476                    | 1.825   | 1.825   | 1.750   | 1.884   | 1.940   |
| Bias  - Bias CL                            | 1.783  | 1.519   | 1.110   | 0.978   | 0.896   | 0.789   |  | 1.606                    | 1.112   | 0.788   | 0.757   | 0.717   | 0.690   |
| Bias  < Bias CL?                           | No     | No      | No      | No      | No      | No      |  | No                       | No      | No      | No      | No      | No      |

Table 4b. (cont'd)

| Digestibility of dry matter <i>in vitro</i> |                           |         |         |         |         |         |                            |         |         |         |         |         |         |
|---|---------------------------|---------|---------|---------|---------|---------|----------------------------|---------|---------|---------|---------|---------|---------|
|   | Step-up Regression 2,2,2  |         |         |         |         |         | Step-up Regression 2,5,5   |         |         |         |         |         |         |
|   | 1 term                    | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 1 term                     | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 6 terms |
| Lowest partial F-ratio                      | 73.30                     | 5.73    | 8.71    | 17.00   | 13.23   | 2.99    | 81.21                      | 12.38   | 8.48    | 7.23    | 6.07    | 3.72    | 3.72    |
| R <sup>2</sup>                              | 0.692                     | 0.733   | 0.788   | 0.863   | 0.905   | 0.915   | 0.715                      | 0.791   | 0.833   | 0.863   | 0.884   | 0.894   | 0.894   |
| SEC   | 3.913                     | 3.645   | 2.251   | 2.610   | 2.177   | 2.058   | 3.768                      | 3.222   | 2.883   | 2.616   | 2.407   | 2.294   | 2.294   |
| SEC CL                                      | 2.420                     | 2.035   | 1.867   | 1.743   | 1.608   | 1.546   | 2.497                      | 1.928   | 1.792   | 1.774   | 1.565   | 1.516   | 1.516   |
| SEV(C)                                      | 4.020                     | 3.186   | 3.411   | 2.781   | 2.324   | 2.203   | 3.855                      | 3.360   | 3.063   | 2.809   | 2.615   | 2.490   | 2.490   |
| r <sup>2</sup>                              | 0.731                     | 0.694   | 0.687   | 0.644   | 0.685   | 0.671   | 0.735                      | 0.856   | 0.845   | 0.849   | 0.801   | 0.800   | 0.800   |
| Bias  | 2.350                     | 2.190   | 1.950   | 1.570   | 1.310   | 1.230   | 2.260                      | 1.930   | 1.730   | 1.570   | 1.440   | 1.380   | 1.380   |
| Bias CL                                     | 5.029                     | 4.684   | 2.893   | 3.354   | 2.798   | 2.645   | 4.842                      | 4.141   | 3.705   | 3.362   | 3.093   | 2.948   | 2.948   |
| SEP (C)                                     | 5.090                     | 4.740   | 4.230   | 3.390   | 2.830   | 2.680   | 4.900                      | 4.190   | 3.750   | 3.400   | 3.130   | 2.980   | 2.980   |
| Slope                                       | 0.946                     | 0.868   | 0.861   | 0.877   | 0.860   | 0.830   | 1.080                      | 0.994   | 1.020   | 0.976   | 0.975   | 0.914   | 0.914   |
| Intercept                                   | 2.000                     | 5.890   | 6.550   | 6.140   | 7.240   | 9.150   | -4.700                     | -0.410  | -1.970  | 0.240   | 0.240   | 4.040   | 4.040   |
| R.S.D.                                      | 3.565                     | 3.601   | 3.842   | 3.882   | 4.143   | 3.895   | 3.576                      | 2.637   | 2.733   | 2.694   | 3.097   | 3.103   | 3.103   |
| Bias  - Bias CL                             | -2.679                    | -2.494  | -0.943  | -1.784  | -1.488  | -1.415  | -2.582                     | -2.211  | -1.975  | -1.792  | -1.653  | -1.568  | -1.568  |
| Bias  < Bias CL?                            | Yes                       | Yes     | Yes     | Yes     | Yes     | Yes     | Yes                        | Yes     | Yes     | Yes     | Yes     | Yes     | Yes     |
| Energy required to digest                   |                           |         |         |         |         |         |                            |         |         |         |         |         |         |
|   | Step-up Regression 2,10,5 |         |         |         |         |         | Step-up Regression 2,10,10 |         |         |         |         |         |         |
|   | 1 term                    | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 1 term                     | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 6 terms |
| Lowest partial F-ratio                      | 25.11                     | 14.92   | 5.87    | 4.42    | 7.61    | 1.89    | 23.54                      | 15.23   | 4.01    | 4.30    | 4.35    | 4.66    | 4.66    |
| R <sup>2</sup>                              | 0.430                     | 0.606   | 0.661   | 0.697   | 0.755   | 0.763   | 0.413                      | 0.598   | 0.641   | 0.678   | 0.721   | 0.755   | 0.755   |
| SEC   | 1.942                     | 1.613   | 1.496   | 1.415   | 1.273   | 1.252   | 1.970                      | 1.631   | 1.541   | 1.460   | 1.358   | 1.274   | 1.274   |
| SEC CL                                      | 2.510                     | 2.084   | 1.933   | 1.829   | 1.645   | 1.618   | 2.546                      | 2.108   | 1.991   | 1.887   | 1.755   | 1.646   | 1.646   |
| SEV(C)                                      | 2.020                     | 1.674   | 1.611   | 1.541   | 1.403   | 1.392   | 2.047                      | 1.689   | 1.612   | 1.569   | 1.494   | 1.411   | 1.411   |
| r <sup>2</sup>                              | 0.273                     | 0.398   | 0.456   | 0.473   | 0.476   | 0.498   | 0.291                      | 0.333   | 0.401   | 0.454   | 0.517   | 0.541   | 0.541   |
| Bias  | 1.170                     | 0.970   | 0.900   | 0.850   | 0.760   | 0.750   | 1.180                      | 0.980   | 0.920   | 0.880   | 0.810   | 0.760   | 0.760   |
| Bias CL                                     | 2.496                     | 2.073   | 1.923   | 1.818   | 1.636   | 1.609   | 2.532                      | 2.096   | 1.980   | 1.876   | 1.745   | 1.637   | 1.637   |
| SEP (C)                                     | 2.520                     | 2.100   | 1.950   | 1.840   | 1.650   | 1.630   | 2.560                      | 2.120   | 2.000   | 1.900   | 1.760   | 1.660   | 1.660   |
| Slope                                       | 0.706                     | 0.723   | 0.717   | 0.707   | 0.610   | 0.616   | 0.737                      | 0.581   | 0.639   | 0.653   | 0.715   | 0.709   | 0.709   |
| Intercept                                   | 4.150                     | 3.950   | 4.320   | 4.260   | 5.620   | 5.440   | 3.720                      | 5.850   | 5.040   | 5.040   | 4.130   | 4.160   | 4.160   |
| R.S.D.                                      | 2.170                     | 2.193   | 2.343   | 2.367   | 2.524   | 2.375   | 2.179                      | 1.607   | 1.666   | 1.644   | 1.889   | 1.893   | 1.893   |
| Bias  - Bias CL                             | -1.326                    | -1.103  | -1.023  | -0.968  | -0.876  | -0.859  | -1.352                     | -1.116  | -1.060  | -0.996  | -0.935  | -0.877  | -0.877  |
| Bias  < Bias CL?                            | Yes                       | Yes     | Yes     | Yes     | Yes     | Yes     | Yes                        | Yes     | Yes     | Yes     | Yes     | Yes     | Yes     |

Table 4b. (cont'd)

| Energy required to comminute |                           |         |         |         |         |         |                            |         |         |         |         |         |
|------------------------------|---------------------------|---------|---------|---------|---------|---------|----------------------------|---------|---------|---------|---------|---------|
|                              | Step-up Regression 2,10,5 |         |         |         |         |         | Step-up Regression 2,10,10 |         |         |         |         |         |
|                              | 1 term                    | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 1 term                     | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms |
| Lowest partial F-ratio       | 76.72                     | 5.31    | 2.76    | 2.16    | 1.68    | 1.01    | 74.85                      | 5.39    | 2.13    | 2.96    | 4.38    | 1.49    |
| R <sup>2</sup>               | 0.703                     | 0.739   | 0.754   | 0.763   | 0.772   | 0.800   | 0.698                      | 0.735   | 0.745   | 0.761   | 0.787   | 0.791   |
| SEC                          | 21.158                    | 19.825  | 19.267  | 18.887  | 18.518  | 17.344  | 21.345                     | 19.977  | 19.611  | 18.982  | 17.929  | 17.768  |
| SEC CL                       | 2.510                     | 2.084   | 1.933   | 1.829   | 1.645   | 1.618   | 2.546                      | 2.108   | 1.991   | 1.887   | 1.755   | 1.646   |
| SEV(C)                       | 21.803                    | 20.707  | 20.279  | 19.690  | 19.499  | 18.691  | 22.033                     | 20.904  | 20.985  | 19.911  | 18.777  | 18.634  |
| r <sup>2</sup>               | 0.460                     | 0.468   | 0.414   | 0.394   | 0.330   | 0.215   | 0.434                      | 0.450   | 0.408   | 0.397   | 0.357   | 0.387   |
| Bias                         | 12.690                    | 11.890  | 11.560  | 11.330  | 11.110  | 10.410  | 12.810                     | 11.990  | 11.700  | 11.390  | 10.760  | 10.660  |
| Bias CL                      | 27.191                    | 25.478  | 24.761  | 24.273  | 23.799  | 22.290  | 27.432                     | 25.674  | 25.203  | 24.395  | 23.042  | 22.835  |
| SEP (C)                      | 27.510                    | 25.770  | 25.050  | 24.550  | 24.070  | 22.550  | 27.750                     | 25.970  | 25.490  | 24.680  | 23.310  | 23.100  |
| Slope                        | 0.793                     | 0.737   | 0.688   | 0.649   | 0.598   | 0.468   | 0.776                      | 0.729   | 0.694   | 0.645   | 0.622   | 0.633   |
| Intercept                    | 18.300                    | 24.500  | 31.800  | 39.600  | 48.100  | 67.100  | 20.200                     | 25.600  | 30.800  | 39.000  | 43.600  | 42.200  |
| R.S.D.                       | 26.610                    | 26.420  | 27.720  | 28.170  | 29.640  | 32.080  | 27.230                     | 26.850  | 27.860  | 28.100  | 29.030  | 28.350  |
| Bias  - Bias CL              | -14.501                   | -13.588 | -13.201 | -12.943 | -12.689 | -11.880 | -14.622                    | -13.684 | -13.503 | -12.282 | -12.175 |         |
| Bias  < Bias CL?             | Yes                       | Yes     | Yes     | Yes     | Yes     | Yes     | Yes                        | Yes     | Yes     | Yes     | Yes     | Yes     |
| Energy required to compress  |                           |         |         |         |         |         |                            |         |         |         |         |         |
|                              | Step-up Regression 2,10,5 |         |         |         |         |         | Step-up Regression 2,10,10 |         |         |         |         |         |
|                              | 1 term                    | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 1 term                     | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms |
| Lowest partial F-ratio       | 8.16                      | 2.24    | 8.06    | 4.06    | 1.97    | 4.98    | 6.50                       | 4.94    | 4.91    | 1.75    | 3.54    | 3.83    |
| R <sup>2</sup>               | 0.183                     | 0.214   | 0.364   | 0.457   | 0.532   | 0.592   | 0.147                      | 0.243   | 0.397   | 0.412   | 0.461   | 0.512   |
| SEC                          | 0.267                     | 0.262   | 0.236   | 0.218   | 0.202   | 0.189   | 0.273                      | 0.257   | 0.230   | 0.227   | 0.217   | 0.207   |
| SEC CL                       | 2.510                     | 2.084   | 1.933   | 1.829   | 1.645   | 1.618   | 2.546                      | 2.108   | 1.991   | 1.887   | 1.755   | 1.646   |
| SEV(C)                       | 0.278                     | 0.275   | 0.252   | 0.235   | 0.218   | 0.210   | 0.283                      | 0.273   | 0.250   | 0.250   | 0.247   | 0.235   |
| r <sup>2</sup>               | 0.010                     | 0.028   | 0.052   | 0.076   | 0.086   | 0.053   | 0.006                      | 0.057   | 0.045   | 0.052   | 0.035   | 0.029   |
| Bias                         | 0.160                     | 0.160   | 0.140   | 0.130   | 0.120   | 0.110   | 0.160                      | 0.150   | 0.140   | 0.140   | 0.130   | 0.120   |
| Bias CL                      | 0.343                     | 0.337   | 0.303   | 0.280   | 0.260   | 0.243   | 0.351                      | 0.330   | 0.296   | 0.292   | 0.279   | 0.266   |
| SEP (C)                      | 0.350                     | 0.340   | 0.310   | 0.280   | 0.260   | 0.250   | 0.360                      | 0.330   | 0.300   | 0.290   | 0.280   | 0.270   |
| Slope                        | 0.127                     | 0.212   | 0.239   | 0.252   | 0.218   | 0.142   | 0.102                      | 0.294   | 0.216   | 0.212   | 0.149   | 0.149   |
| Intercept                    | 3.270                     | 2.960   | 2.850   | 2.800   | 2.930   | 3.210   | 3.360                      | 2.640   | 2.940   | 2.950   | 3.180   | 3.190   |
| R.S.D.                       | 0.234                     | 0.233   | 0.235   | 0.236   | 1.942   | 1.495   | 1.736                      | 1.938   | 1.980   | 2.030   | 2.179   | 2.183   |
| Bias  - Bias CL              | -0.183                    | -0.177  | -0.163  | -0.150  | -0.140  | -0.133  | -0.191                     | -0.180  | -0.156  | -0.152  | -0.149  | -0.146  |
| Bias  < Bias CL?             | Yes                       | Yes     | Yes     | Yes     | Yes     | Yes     | Yes                        | Yes     | Yes     | Yes     | Yes     | Yes     |

Table 4b. (cont'd)

| Digestibility of dry matter <i>in vivo</i>  |                           |         |         |         |         |         |                            |         |         |         |         |         |
|---|---------------------------|---------|---------|---------|---------|---------|----------------------------|---------|---------|---------|---------|---------|
|   | Step-up Regression 2,10,5 |         |         |         |         |         | Step-up Regression 2,10,10 |         |         |         |         |         |
|   | 1 term                    | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 1 term                     | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms |
| Lowest partial F-ratio                      | 91.59                     | 9.46    | 9.77    | 7.10    | 2.58    | 4.12    | 93.60                      | 6.52    | 16.07   | 4.36    | 4.68    | 4.94    |
| R <sup>2</sup>                              | 0.700                     | 0.867   | 0.902   | 0.916   | 0.927   | 0.935   | 0.675                      | 0.815   | 0.898   | 0.912   | 0.922   | 0.927   |
| SEC   | 3.139                     | 2.095   | 1.794   | 1.660   | 1.545   | 1.457   | 3.271                      | 2.467   | 1.828   | 1.698   | 1.598   | 1.546   |
| SEC CL                                      | 2.510                     | 2.084   | 1.933   | 1.829   | 1.645   | 1.618   | 2.546                      | 2.108   | 1.991   | 1.887   | 1.755   | 1.646   |
| SEV(C)                                      | 3.332                     | 2.282   | 1.997   | 1.830   | 1.694   | 1.607   | 3.357                      | 2.572   | 2.016   | 1.905   | 1.840   | 1.787   |
| r <sup>2</sup>                              | 0.777                     | 0.856   | 0.888   | 0.871   | 0.887   | 0.881   | 0.828                      | 0.831   | 0.809   | 0.836   | 0.877   | 0.892   |
| Bias  | 1.880                     | 1.260   | 1.080   | 1.000   | 0.930   | 0.870   | 1.960                      | 1.480   | 1.100   | 1.020   | 0.960   | 0.930   |
| Bias CL                                     | 0.343                     | 0.337   | 0.303   | 0.280   | 0.260   | 0.243   | 0.351                      | 0.330   | 0.296   | 0.292   | 0.279   | 0.266   |
| SEP(C)                                      | 4.080                     | 2.720   | 2.330   | 2.160   | 2.010   | 1.890   | 4.250                      | 3.210   | 2.380   | 2.210   | 2.080   | 2.010   |
| Slope                                       | 0.892                     | 0.880   | 0.924   | 0.870   | 0.851   | 0.837   | 1.130                      | 0.991   | 0.812   | 0.829   | 0.840   | 0.865   |
| Intercept                                   | 7.380                     | 6.750   | 3.930   | 6.850   | 8.320   | 8.960   | -6.490                     | 0.210   | 9.960   | 9.030   | 8.710   | 7.270   |
| R.S.D.                                      | 2.531                     | 2.034   | 1.791   | 1.927   | 1.799   | 1.848   | 2.222                      | 2.201   | 2.344   | 2.172   | 1.876   | 1.761   |
| Bias  - Bias CL                             | 1.537                     | 0.923   | 0.777   | 0.720   | 0.670   | 0.627   | 1.609                      | 1.150   | 0.804   | 0.728   | 0.681   | 0.664   |
| Bias  < Bias CL?                            | No                        | No      | No      | No      | No      | No      | No                         | No      | No      | No      | No      | No      |
| Digestibility of dry matter <i>in vitro</i> |                           |         |         |         |         |         |                            |         |         |         |         |         |
|   | Step-up Regression 2,10,5 |         |         |         |         |         | Step-up Regression 2,10,10 |         |         |         |         |         |
|   | 1 term                    | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms | 1 term                     | 2 terms | 3 terms | 4 terms | 5 terms | 6 terms |
| Lowest partial F-ratio                      | 94.12                     | 6.62    | 16.01   | 4.48    | 4.61    | 5.01    | 92.14                      | 9.60    | 9.70    | 10.55   | 2.67    | 4.41    |
| R <sup>2</sup>                              | 0.744                     | 0.784   | 0.856   | 0.871   | 0.886   | 0.901   | 0.740                      | 0.797   | 0.842   | 0.881   | 0.888   | 0.900   |
| SEC   | 3.568                     | 3.283   | 2.680   | 2.532   | 2.384   | 2.224   | 3.596                      | 3.182   | 2.802   | 2.430   | 2.361   | 2.235   |
| SEC CL                                      | 2.510                     | 2.084   | 1.933   | 1.829   | 1.645   | 1.618   | 2.546                      | 2.108   | 1.991   | 1.887   | 1.755   | 1.646   |
| SEV(C)                                      | 3.633                     | 3.371   | 2.785   | 2.667   | 2.563   | 2.364   | 3.655                      | 3.280   | 2.892   | 2.618   | 2.525   | 2.416   |
| r <sup>2</sup>                              | 0.828                     | 0.816   | 0.813   | 0.802   | 0.819   | 0.851   | 0.823                      | 0.807   | 0.810   | 0.844   | 0.818   | 0.823   |
| Bias  | 2.140                     | 1.970   | 1.610   | 1.520   | 1.430   | 1.330   | 2.160                      | 1.910   | 1.680   | 1.460   | 1.420   | 1.340   |
| Bias CL                                     | 4.585                     | 4.219   | 3.444   | 3.254   | 3.064   | 2.858   | 4.621                      | 4.089   | 3.601   | 3.123   | 3.034   | 2.872   |
| SEP(C)                                      | 4.640                     | 4.270   | 3.480   | 3.290   | 3.100   | 2.890   | 4.680                      | 4.140   | 3.640   | 3.160   | 3.070   | 2.910   |
| Slope                                       | 0.960                     | 0.971   | 0.906   | 0.862   | 0.867   | 0.864   | 0.937                      | 0.927   | 0.882   | 0.935   | 0.881   | 0.841   |
| Intercept                                   | 2.120                     | 1.280   | 4.530   | 7.230   | 7.380   | 7.610   | 3.490                      | 3.660   | 5.790   | 3.260   | 6.140   | 8.660   |
| R.S.D.                                      | 2.978                     | 3.002   | 3.088   | 2.952   | 2.681   | 2.922   | 3.023                      | 2.742   | 2.959   | 2.846   | 0.231   | 0.239   |
| Bias  - Bias CL                             | -2.445                    | -2.249  | -1.834  | -1.734  | -1.634  | -1.528  | -2.461                     | -2.179  | -1.921  | -1.663  | -1.614  | -1.532  |
| Bias  < Bias CL?                            | Yes                       | Yes     | Yes     | Yes     | Yes     | Yes     | Yes                        | Yes     | Yes     | Yes     | Yes     | Yes     |

Table 4c. Calibration and validation statistics (multivariate regressions)

| Energy required to shear     |         |         |         |         |         |         |
|------------------------------|---------|---------|---------|---------|---------|---------|
|                              | PCR     |         | PLS     |         | MPLS    |         |
|                              | 2.5,5   | 2.10,10 | 2.5,5   | 2.10,10 | 2.5,5   | 2.10,10 |
| R <sup>2</sup>               | 0.847   | 0.752   | 0.639   | 0.601   | 0.601   | 0.582   |
| SEC                          | 1.036   | 1.290   | 1.545   | 1.624   | 1.550   | 1.586   |
| SEC CL                       | 1.199   | 1.493   | 1.788   | 1.879   | 1.793   | 1.835   |
| SECV                         | 1.750   | 1.592   | 1.788   | 1.933   | 1.600   | 1.583   |
| r <sup>2</sup>               | 0.5441  | 0.4876  | 0.4938  | 0.4157  | 0.3080  | 0.3563  |
| Bias                         | 0.620   | 0.770   | 0.930   | 0.970   | 0.930   | 0.950   |
| Bias CL                      | 1.331   | 1.658   | 1.986   | 2.087   | 1.992   | 2.038   |
| SEP (C)                      | 1.350   | 1.680   | 2.010   | 2.110   | 2.020   | 2.060   |
| Slope                        | 0.6540  | 0.6850  | 0.7390  | 0.6270  | 0.5220  | 0.6000  |
| Intercept                    | 5.2900  | 4.8100  | 3.7500  | 5.4500  | 7.3100  | 6.0200  |
| R.S.D.                       | 1.671   | 1.776   | 1.761   | 1.892   | 2.065   | 1.992   |
| Bias  - Bias CL              | -0.711  | -0.888  | -1.056  | -1.117  | -1.062  | -1.088  |
| Bias  < Bias CL?             | Yes     | Yes     | Yes     | Yes     | Yes     | Yes     |
| Energy required to comminute |         |         |         |         |         |         |
|                              | PCR     |         | PLS     |         | MPLS    |         |
|                              | 2.5,5   | 2.10,10 | 2.5,5   | 2.10,10 | 2.5,5   | 2.10,10 |
| R <sup>2</sup>               | 0.584   | 0.574   | 0.605   | 0.595   | 0.556   | 0.558   |
| SEC                          | 23.378  | 23.682  | 22.788  | 23.075  | 24.164  | 24.101  |
| SEC CL                       | 27.048  | 27.400  | 26.366  | 26.698  | 27.958  | 27.885  |
| SECV                         | 26.030  | 26.121  | 25.548  | 25.683  | 26.409  | 26.252  |
| r <sup>2</sup>               | 0.349   | 0.337   | 0.332   | 0.325   | 0.33    | 0.328   |
| Bias                         | 14.030  | 14.210  | 13.670  | 13.840  | 14.500  | 14.460  |
| Bias CL                      | 30.044  | 30.435  | 29.286  | 29.655  | 31.055  | 30.974  |
| SEP (C)                      | 30.390  | 30.790  | 29.620  | 30.000  | 31.410  | 31.330  |
| Slope                        | 0.649   | 0.636   | 0.644   | 0.632   | 0.657   | 0.638   |
| Intercept                    | 37.3    | 39.2    | 38.1    | 39.7    | 36.6    | 39.1    |
| R.S.D.                       | 28.246  | 28.676  | 28.714  | 28.884  | 28.651  | 28.900  |
| Bias  - Bias CL              | -16.014 | -16.225 | -15.616 | -15.815 | -16.555 | -16.514 |
| Bias  < Bias CL?             | Yes     | Yes     | Yes     | Yes     | Yes     | Yes     |
| Energy required to compress  |         |         |         |         |         |         |
|                              | PCR     |         | PLS     |         | MPLS    |         |
|                              | 2.5,5   | 2.10,10 | 2.5,5   | 2.10,10 | 2.5,5   | 2.10,10 |
| R <sup>2</sup>               | 0.251   | 0.160   | 0.231   | 0.208   | 0.038   | 0.040   |
| SEC                          | 0.225   | 0.241   | 0.265   | 0.269   | 0.260   | 0.260   |
| SEC CL                       | 0.260   | 0.279   | 0.307   | 0.311   | 0.301   | 0.301   |
| SECV                         | 0.299   | 0.277   | 0.301   | 0.307   | 0.301   | 0.299   |
| r <sup>2</sup>               | 0.0220  | 0.0120  | 0.0130  | 0.0090  | 0.0060  | 0.0080  |
| Bias                         | 0.140   | 0.140   | 0.160   | 0.160   | 0.160   | 0.160   |
| Bias CL                      | 0.289   | 0.310   | 0.341   | 0.346   | 0.334   | 0.334   |
| SEP (C)                      | 0.290   | 0.310   | 0.340   | 0.350   | 0.340   | 0.340   |
| Slope                        | 0.2290  | 0.2270  | 0.1530  | 0.1330  | 0.2290  | 0.2590  |
| Intercept                    | 2.8900  | 2.9000  | 3.1700  | 3.2500  | 2.8900  | 2.7700  |
| R.S.D.                       | 0.235   | 0.236   | 0.236   | 0.237   | 0.237   | 0.237   |
| Bias  - Bias CL              | -0.149  | -0.170  | -0.181  | -0.186  | -0.174  | -0.174  |
| Bias  < Bias CL?             | Yes     | Yes     | Yes     | Yes     | Yes     | Yes     |

Table 4c (cont'd) Calibration and validation statistics  
(multivariate regressions)

| Digestibility of dry matter <i>in vivo</i>  |        |         |        |         |         |         |
|---|--------|---------|--------|---------|---------|---------|
|   | PCR    |         | PLS    |         | MPLS    |         |
|   | 2.5,5  | 2.10,10 | 2.5,5  | 2.10,10 | 2.5,5   | 2.10,10 |
| R <sup>2</sup>                              | 0.909  | 0.900   | 0.958  | 0.937   | 0.571   | 0.892   |
| SEC   | 1.638  | 1.711   | 1.109  | 1.356   | 3.756   | 1.911   |
| SEC CL                                      | 1.895  | 1.980   | 1.283  | 1.569   | 4.346   | 2.211   |
| SECV  | 2.159  | 2.075   | 1.957  | 1.776   | 3.797   | 2.180   |
| r <sup>2</sup>                              | 0.9022 | 0.8865  | 0.8447 | 0.8457  | 0.6963  | 0.8671  |
| Bias  | 0.980  | 1.030   | 0.670  | 0.810   | 2.250   | 1.150   |
| Bias CL                                     | 2.105  | 2.199   | 1.425  | 1.743   | 4.827   | 2.456   |
| SEP (C)                                     | 2.130  | 2.220   | 1.440  | 1.760   | 4.880   | 2.480   |
| Slope                                       | 0.848  | 0.807   | 0.839  | 0.822   | 0.981   | 0.745   |
| Intercept                                   | 8.77   | 11.1    | 8.65   | 9.41    | 1.99    | 14.6    |
| R.S.D.                                      | 1.704  | 1.834   | 2.143  | 2.139   | 2.914   | 1.984   |
| Bias  - Bias CL                             | -1.125 | -1.169  | -0.755 | -0.933  | -2.577  | -1.306  |
| Bias  < Bias CL?                            | Yes    | Yes     | Yes    | Yes     | Yes     | Yes     |
| Digestibility of dry matter <i>in vitro</i> |        |         |        |         |         |         |
|   | PCR    |         | PLS    |         | MPLS    |         |
|   | 2.5,5  | 2.10,10 | 2.5,5  | 2.10,10 | 2.5,5   | 2.10,10 |
| R <sup>2</sup>                              | 0.820  | 0.790   | 0.780  | 0.760   | 0.420   | 0.490   |
| SEC   | 2.880  | 3.100   | 3.330  | 3.470   | 5.380   | 4.850   |
| SEC CL                                      | 3.332  | 3.587   | 3.853  | 4.015   | 6.225   | 5.611   |
| SECV  | 3.170  | 3.560   | 3.830  | 3.900   | 5.690   | 4.780   |
| r <sup>2</sup>                              | 0.8120 | 0.7730  | 0.8530 | 0.8040  | 0.6910  | 0.6690  |
| Bias  | 1.730  | 1.860   | 2.000  | 2.080   | 3.230   | 2.910   |
| Bias CL                                     | 3.701  | 3.984   | 4.280  | 4.459   | 6.914   | 6.233   |
| SEP (C)                                     | 3.740  | 4.030   | 4.330  | 4.510   | 6.990   | 6.310   |
| Slope                                       | 0.9180 | 0.9840  | 0.9530 | 0.6120  | 1.1200  | 0.8650  |
| Intercept                                   | 3.4700 | -0.3600 | 2.3100 | 4.6300  | -7.5100 | 6.1800  |
| R.S.D.                                      | 3.053  | 3.363   | 2.836  | 3.089   | 3.911   | 4.002   |
| Bias  - Bias CL                             | -1.971 | -2.124  | -2.280 | -2.379  | -3.684  | -3.323  |
| Bias  < Bias CL?                            | Yes    | Yes     | Yes    | Yes     | Yes     | Yes     |



Table 5. Standard error of laboratory determination (SEL)

|                           | Energy<br>required to<br>shear<br>(kJ/m <sup>2</sup> ) | Energy<br>required to<br>comminute<br>(kJ/kg DM) | Energy<br>required to<br>compress<br>(kJ/kg DM) | Digestibility<br>of dry<br>matter<br><i>in vivo</i><br>(%) | Digestibility<br>of dry<br>matter<br><i>in vitro</i><br>(%) |
|---------------------------|--|--|---|--|---|
| Mean SEL (n=65)           | 0.796  | 5.830  | 0.078   | not available  | 0.314   |
| Median SEL                | 0.788  | 5.492  | 0.085   | not available  | 0.270   |
| Maximum SEL               | 2.044  | 13.098   | 0.211   | not available  | 1.128   |
| Minimum SEL               | 0.114  | 0.760  | 0.019   | not available  | 0.005   |
| SEL CL (using mean SEL)   | 1.035  | 7.319  | 0.101   | not available  | 0.408   |
| SEL CL (using median SEL) | 1.024  | 7.140  | 0.111   | not available  | 0.351   |

Table 6a. Components of possible prediction equations from stepwise and step-up regression analyses.

|   | Coefficient         | Wavelength | Coefficient       | Wavelength |
|---|---------------------|------------|-------------------|------------|
| Energy required to shear                    |                     |            |                   |            |
| Regression analysis                         | Stepwise            |            | Step-up           |            |
| Mathematical treatment                      | 2,2,2 (8 terms)     |            | 2,5,5 (2 terms)   |            |
|   | 18.95               |            | 28.09             |            |
|   | 2452.05             | 2048       | 1035.77           | 2048       |
|   | <del>-258.61</del>  | 1988       | 700.12            | 1858       |
|   | 3223.49             | 1458       |                   |            |
|   | <del>-5319.88</del> | 1718       |                   |            |
|   | 5149.38             | 1828       |                   |            |
|   | 10239.43            | 1188       |                   |            |
| Energy required to compress                 |                     |            |                   |            |
| Regression analysis                         | Stepwise            |            | Step-up           |            |
| Mathematical treatment                      | 2,10,10 (4 terms)   |            | 2,10,5 (3 terms)  |            |
|   | -0.71               |            | 2.49              |            |
|   | -28.02              | 2278       | -31.05            | 1728       |
|   | 112.57              | 1588       | -108.89           | 1548       |
|   | -78.48              | 1728       | -405.95           | 1238       |
|   | -811.04             | 1238       |                   |            |
| Energy required to comminute                |                     |            |                   |            |
| Regression analysis                         | Stepwise            |            | Step-up           |            |
| Mathematical treatment                      | 2,10,5 (4 terms)    |            | 2,10,5 (1 term)   |            |
|   | 231.42              |            | -69.08            |            |
|   | <del>-3003.37</del> | 2128       | -1521.33          | 2238       |
|   | <del>-280.19</del>  | 2408       |                   |            |
|   | <del>-4853.12</del> | 2018       |                   |            |
|   | 18224.74            | 1138       |                   |            |
| Digestibility of dry matter <i>in vivo</i>  |                     |            |                   |            |
| Regression analysis                         | Stepwise            |            | Step-up           |            |
| Mathematical treatment                      | 2,5,5 (8 terms)     |            | 2,10,5 (3 terms)  |            |
|   | 48.82               |            | 48.18             |            |
|   | -337.08             | 1818       | -812.43           | 1698       |
|   | -9799.89            | 1238       | 252.82            | 1418       |
|   | 8162.72             | 1158       | -943.77           | 1818       |
|   | 1249.01             | 1688       |                   |            |
|   | 518.48              | 1908       |                   |            |
|   | -181.84             | 2248       |                   |            |
| Digestibility of dry matter <i>in vitro</i> |                     |            |                   |            |
| Regression analysis                         | Stepwise            |            | Step-up           |            |
| Mathematical treatment                      | 2,5,5 (5 terms)     |            | 2,10,10 (4 terms) |            |
|   | 63.43               |            | 54.29             |            |
|   | -958.01             | 1818       | -1171.70          | 1698       |
|   | 981.30              | 1908       | 311.12            | 1418       |
|   | -2188.89            | 1688       | -2857.69          | 1818       |
|   | 2003.05             | 2158       | -2319.81          | 1228       |
|   | -1481.99            | 1748       |                   |            |

Table 6b. Components of possible prediction equations from multivariate regression analyses.

| Energy required to shear<br>PCR (2,5,6) |            | Energy required to compress<br>PCR (2,5,6) |            | Energy required to comminute<br>PCR (2,5,6) |            | PLS (2,5,6) |            |
|---|------------|--|------------|---|------------|-------------|------------|
| Coefficient                             | Wavelength | Coefficient                                | Wavelength | Coefficient                                 | Wavelength | Coefficient | Wavelength |
| -3.33                                   | 1108       | 3.35                                       | 1108       | -22.8                                       | 1108       | -16.44      | 1108       |
| 18.1                                    | 1118       | 0.17                                       | 1118       | 93.07                                       | 1118       | 91.01       | 1118       |
| 1.78                                    | 1128       | 0.02                                       | 1128       | 6.5   | 1128       | 7.19        | 1128       |
| -0.2                                    | 1138       | -0.01                                      | 1138       | -7.27                                       | 1138       | -5.63       | 1138       |
| -0.84                                   | 1148       | -0.01                                      | 1148       | -0.79                                       | 1148       | -0.13       | 1148       |
| 1.15                                    | 1158       | 0.01                                       | 1158       | 3.98  | 1158       | 5.58        | 1158       |
| -0.85                                   | 1168       | -0.01                                      | 1168       | -10.39                                      | 1168       | -8.55       | 1168       |
| 0.13                                    | 1178       | 0  | 1178       | -4.8  | 1178       | -4.72       | 1178       |
| 0.64                                    | 1188       | 0.03                                       | 1188       | 13.75                                       | 1188       | 13.27       | 1188       |
| -0.04                                   | 1198       | 0.04                                       | 1198       | 19.07                                       | 1198       | 17.38       | 1198       |
| -0.84                                   | 1208       | 0  | 1208       | 5.08  | 1208       | 0.44        | 1208       |
| -1.14                                   | 1218       | -0.03                                      | 1218       | -8.92                                       | 1218       | -13.98      | 1218       |
| -1.71                                   | 1228       | -0.05                                      | 1228       | -20.63                                      | 1228       | -23.8       | 1228       |
| -1.73                                   | 1238       | -0.04                                      | 1238       | -17.9                                       | 1238       | -15.15      | 1238       |
| -0.85                                   | 1248       | -0.01                                      | 1248       | -3.28                                       | 1248       | -0.82       | 1248       |
| 0.12                                    | 1258       | 0  | 1258       | -0.85                                       | 1258       | 1.6         | 1258       |
| 0.5                                     | 1268       | 0  | 1268       | -2.55                                       | 1268       | -0.82       | 1268       |
| -0.9                                    | 1278       | -0.01                                      | 1278       | -4.67                                       | 1278       | -3.84       | 1278       |
| -1.25                                   | 1288       | 0  | 1288       | 1.29  | 1288       | 1.1         | 1288       |
| -0.25                                   | 1298       | 0.01                                       | 1298       | 5.24  | 1298       | 4.93        | 1298       |
| 0.2                                     | 1308       | 0.02                                       | 1308       | 5.9   | 1308       | 7.12        | 1308       |
| -0.1                                    | 1318       | 0.03                                       | 1318       | 9.22  | 1318       | 10.4        | 1318       |
| -0.68                                   | 1328       | 0.04                                       | 1328       | 14.28                                       | 1328       | 16.14       | 1328       |
| 1.25                                    | 1338       | 0.06                                       | 1338       | 22.7  | 1338       | 23.58       | 1338       |
| 5                                       | 1348       | 0.07                                       | 1348       | 27.63                                       | 1348       | 27.65       | 1348       |
| 2.34                                    | 1358       | 0.03                                       | 1358       | 6.84  | 1358       | 10.27       | 1358       |
| -2.37                                   | 1368       | -0.06                                      | 1368       | -26.23                                      | 1368       | -24.35      | 1368       |
| -10.62                                  | 1378       | -0.15                                      | 1378       | -66.38                                      | 1378       | -60.7       | 1378       |
| -9.89                                   | 1388       | -0.01                                      | 1388       | -1.83                                       | 1388       | 2.2         | 1388       |
| -1.68                                   | 1398       | 0.16                                       | 1398       | 67.77                                       | 1398       | 67.91       | 1398       |
| 8.65                                    | 1408       | 0.3  | 1408       | 125.67                                      | 1408       | 115.99      | 1408       |
| 23.88                                   | 1418       | 0.49                                       | 1418       | 188.24                                      | 1418       | 174.79      | 1418       |
| 13.87                                   | 1428       | 0.2  | 1428       | 67.19                                       | 1428       | 62.69       | 1428       |
| -12.53                                  |            | -0.37                                      |            | -153.54                                     |            | -139.99     |            |

SUBSTITUTE SHEET (RULE 26)

Table 6b. Components of possible prediction equations from multivariate regression analyses.

| Energy required to shear<br>PCR (2,5,6) |            | Energy required to compress<br>PCR (2,5,6) |            | Energy required to comminute<br>PCR (2,5,6) |            | PLS (2,5,6) |            |
|---|------------|--|------------|---|------------|-------------|------------|
| Coefficient                             | Wavelength | Coefficient                                | Wavelength | Coefficient                                 | Wavelength | Coefficient | Wavelength |
| -10.01                                  | 1438       | -0.39                                      | 1438       | -145.28                                     | 1438       | -137.82     | 1438       |
| -1.04                                   | 1448       | -0.21                                      | 1448       | -68.74                                      | 1448       | -75.27      | 1448       |
| 2.09                                    | 1458       | -0.13                                      | 1458       | -37.31                                      | 1458       | -47.38      | 1458       |
| -2.89                                   | 1468       | -0.11                                      | 1468       | -49.09                                      | 1468       | -48.54      | 1468       |
| -8.05                                   | 1478       | -0.14                                      | 1478       | -70.4                                       | 1478       | -59.84      | 1478       |
| -1.2                                    | 1488       | -0.08                                      | 1488       | -28.84                                      | 1488       | -28.08      | 1488       |
| -2.08                                   | 1498       | -0.01                                      | 1498       | -1.87                                       | 1498       | -3.2        | 1498       |
| -1.69                                   | 1508       | 0.01                                       | 1508       | 4.61  | 1508       | 3.33        | 1508       |
| 0.35                                    | 1518       | 0.07                                       | 1518       | 28.89                                       | 1518       | 28.91       | 1518       |
| 2.8                                     | 1528       | 0.12                                       | 1528       | 49.84                                       | 1528       | 48.03       | 1528       |
| -0.01                                   | 1538       | 0.08                                       | 1538       | 34.38                                       | 1538       | 33.02       | 1538       |
| -1.83                                   | 1548       | 0  | 1548       | -3.32                                       | 1548       | 0.49        | 1548       |
| -3.7                                    | 1558       | -0.04                                      | 1558       | -21.79                                      | 1558       | -17.62      | 1558       |
| -0.66                                   | 1568       | -0.01                                      | 1568       | -4.61                                       | 1568       | -3.35       | 1568       |
| -1.99                                   | 1578       | -0.04                                      | 1578       | -13.08                                      | 1578       | -15.39      | 1578       |
| -3.97                                   | 1588       | -0.09                                      | 1588       | -43.91                                      | 1588       | -40.21      | 1588       |
| -5.28                                   | 1598       | -0.07                                      | 1598       | -30.2                                       | 1598       | -32.77      | 1598       |
| 0.08                                    | 1608       | -0.01                                      | 1608       | -7.28                                       | 1608       | -5.93       | 1608       |
| 2.89                                    | 1618       | 0.04                                       | 1618       | 17.4  | 1618       | 15          | 1618       |
| 0.22                                    | 1628       | 0.09                                       | 1628       | 34.68                                       | 1628       | 33.13       | 1628       |
| -0.98                                   | 1638       | 0.13                                       | 1638       | 49.47                                       | 1638       | 48.83       | 1638       |
| 18.23                                   | 1648       | 0.1  | 1648       | 53.35                                       | 1648       | 44.32       | 1648       |
| 10.67                                   | 1658       | 0  | 1658       | -3.16                                       | 1658       | -2.24       | 1658       |
| 6.52                                    | 1668       | -0.22                                      | 1668       | -82.09                                      | 1668       | -80.94      | 1668       |
| -20.53                                  | 1678       | -0.07                                      | 1678       | -60.38                                      | 1678       | -36.22      | 1678       |
| -6.15                                   | 1688       | 0.15                                       | 1688       | 55.85                                       | 1688       | 60.49       | 1688       |
| 7.4                                     | 1698       | 0.08                                       | 1698       | 48.43                                       | 1698       | 42.6        | 1698       |
| 4.76                                    | 1708       | 0.08                                       | 1708       | 34.19                                       | 1708       | 27.79       | 1708       |
| -19.73                                  | 1718       | -0.09                                      | 1718       | -54.88                                      | 1718       | -48.38      | 1718       |
| -5.98                                   | 1728       | -0.13                                      | 1728       | -54.89                                      | 1728       | -69.44      | 1728       |
| 19.24                                   | 1738       | 0.15                                       | 1738       | 78.27                                       | 1738       | 63.67       | 1738       |
| 6.42                                    | 1748       | 0.19                                       | 1748       | 80.94                                       | 1748       | 91.13       | 1748       |
| -3.1                                    | 1758       | 0.08                                       | 1758       | 21.41                                       | 1758       | 20.27       | 1758       |
| -4.03                                   | 1768       | -0.1                                       | 1768       | -47.2                                       | 1768       | -48.58      | 1768       |
| -1.47                                   | 1778       | -0.11                                      | 1778       | -42.48                                      | 1778       | -39.05      | 1778       |
| -0.44                                   | 1788       | -0.09                                      | 1788       | -38.22                                      | 1788       | -33.03      | 1788       |
| 1.72                                    | 1798       | -0.01                                      | 1798       | -2.33                                       | 1798       | -3.76       | 1798       |

Table 6b. Components of possible prediction equations from multivariate regression analyses.

| Energy required to shear |            |  | Energy required to compress |            |  | Energy required to comminute |            |         |
|--------------------------|------------|--|-----------------------------|------------|--|------------------------------|------------|---------|
| PCR (2,5,6)              |            |  | PCR (2,5,6)                 |            |  | PCR (2,5,6)                  |            |         |
| Coefficient              | Wavelength |  | Coefficient                 | Wavelength |  | Coefficient                  | Wavelength |         |
| 2.78                     | 1808       |  | 0.05                        | 1808       |  | 20.97                        | 1808       | 18.41   |
| -3.79                    | 1818       |  | -0.01                       | 1818       |  | -8.58                        | 1818       | -5.17   |
| -4.32                    | 1828       |  | -0.07                       | 1828       |  | -30.81                       | 1828       | -28.5   |
| -2.97                    | 1838       |  | -0.05                       | 1838       |  | -17.29                       | 1838       | -17.64  |
| 1.97                     | 1848       |  | 0.03                        | 1848       |  | 17.65                        | 1848       | 15.59   |
| -2.48                    | 1858       |  | 0.08                        | 1858       |  | 28.08                        | 1858       | 28.11   |
| -6.48                    | 1868       |  | 0.08                        | 1868       |  | 42.2                         | 1868       | 40.46   |
| -10.22                   | 1878       |  | 0.23                        | 1878       |  | 115.52                       | 1878       | 108.88  |
| -1.84                    | 1888       |  | 0.44                        | 1888       |  | 219.15                       | 1888       | 208.1   |
| 31.11                    | 1898       |  | 0.2                         | 1898       |  | 88.82                        | 1898       | 89.42   |
| 2.3                      | 1908       |  | -0.35                       | 1908       |  | -179.9                       | 1908       | -157.11 |
| -25.69                   | 1918       |  | -0.47                       | 1918       |  | -251.3                       | 1918       | -220.58 |
| -12.22                   | 1928       |  | -0.34                       | 1928       |  | -171.83                      | 1928       | -172.09 |
| 15.11                    | 1938       |  | -0.14                       | 1938       |  | -55.38                       | 1938       | -77.27  |
| 28.89                    | 1948       |  | -0.03                       | 1948       |  | -8.17                        | 1948       | -23.21  |
| 27.72                    | 1958       |  | -0.04                       | 1958       |  | -18.85                       | 1958       | -19.03  |
| 8.93                     | 1968       |  | 0.05                        | 1968       |  | 12.02                        | 1968       | 22.48   |
| -15.33                   | 1978       |  | 0.23                        | 1978       |  | 68.03                        | 1978       | 88.86   |
| -9.25                    | 1988       |  | 0.29                        | 1988       |  | 85.84                        | 1988       | 103.8   |
| -3.33                    | 1998       |  | 0.27                        | 1998       |  | 78.88                        | 1998       | 88.03   |
| 1.28                     | 2008       |  | 0.32                        | 2008       |  | 97.53                        | 2008       | 115.14  |
| 20.22                    | 2018       |  | 0.25                        | 2018       |  | 104.79                       | 2018       | 99.25   |
| 18.34                    | 2028       |  | 0.08                        | 2028       |  | 42.06                        | 2028       | 33.39   |
| 9.58                     | 2038       |  | -0.01                       | 2038       |  | 23.88                        | 2038       | 11.1    |
| 5.59                     | 2048       |  | 0.13                        | 2048       |  | 101.85                       | 2048       | 77.38   |
| -8.54                    | 2058       |  | 0.21                        | 2058       |  | 128.79                       | 2058       | 109.6   |
| -18.75                   | 2068       |  | -0.2                        | 2068       |  | -75.99                       | 2068       | -71.48  |
| -18.33                   | 2078       |  | -0.48                       | 2078       |  | -208.62                      | 2078       | -188.9  |
| -10.13                   | 2088       |  | -0.38                       | 2088       |  | -151.16                      | 2088       | -143.85 |
| -5.78                    | 2098       |  | -0.28                       | 2098       |  | -107.24                      | 2098       | -104.89 |
| -8.44                    | 2108       |  | -0.28                       | 2108       |  | -108.08                      | 2108       | -107.49 |
| -6.28                    | 2118       |  | -0.23                       | 2118       |  | -91.08                       | 2118       | -91.23  |
| -4.49                    | 2128       |  | -0.23                       | 2128       |  | -97.55                       | 2128       | -93.37  |
| -18.58                   | 2138       |  | -0.2                        | 2138       |  | -101.35                      | 2138       | -85.08  |
| -9.08                    | 2148       |  | -0.01                       | 2148       |  | -13.78                       | 2148       | -9.31   |
| -2.88                    | 2158       |  | 0.08                        | 2158       |  | 37.5                         | 2158       | 36.99   |
| 3.19                     | 2168       |  | 0.28                        | 2168       |  | 118.43                       | 2168       | 110.03  |

SUBSTITUTE SHEET (RULE 26)

Table 6b. Components of possible prediction equations from multivariate regression analyses.

| Energy required to shear<br>PCR (2,5,5) |            | Energy required to compress<br>PCR (2,5,5) |            | Energy required to comminute<br>PLS (2,5,5) |            |
|---|------------|--|------------|---|------------|
| Coefficient                             | Wavelength | Coefficient                                | Wavelength | Coefficient                                 | Wavelength |
| 4.27                                    | 2178       | 0.28                                       | 2178       | 122.68                                      | 2178       |
| -6.3                                    | 2188       | 0.16                                       | 2188       | 54.73                                       | 2188       |
| -13.33                                  | 2198       | 0.15                                       | 2198       | 38.08                                       | 2188       |
| -2.74                                   | 2208       | 0.35                                       | 2208       | 129.58                                      | 2188       |
| 35.77                                   | 2218       | 0.38                                       | 2218       | 171.77                                      | 2208       |
| 30.36                                   | 2228       | 0.42                                       | 2228       | 182.8                                       | 2218       |
| 22.91                                   | 2238       | 0.22                                       | 2238       | 73.19                                       | 2228       |
| 98.91                                   | 2248       | -0.67                                      | 2248       | -152.9                                      | 2238       |
| -15.77                                  | 2258       | -0.47                                      | 2258       | -184.5                                      | 2248       |
| -85.22                                  | 2268       | -0.2                                       | 2268       | -187.23                                     | 2258       |
| -35.1                                   | 2278       | -0.45                                      | 2278       | -214.87                                     | 2268       |
| 27.27                                   | 2288       | 0.22                                       | 2288       | 1.48  | 2278       |
| 4.27                                    | 2298       | 0.64                                       | 2298       | 352.88                                      | 2288       |
| -13.08                                  | 2308       | 0.29                                       | 2308       | 78.88                                       | 2298       |
| 0.87                                    | 2318       | -0.48                                      | 2318       | -208.27                                     | 2308       |
| -13.34                                  | 2328       | -0.47                                      | 2328       | -187.95                                     | 2318       |
| -23.3                                   | 2338       | -0.2                                       | 2338       | -78.26                                      | 2328       |
| 0.66                                    | 2348       | 0.15                                       | 2348       | 62.44                                       | 2338       |
| 7.98                                    | 2358       | -0.07                                      | 2358       | -23.09                                      | 2348       |
| -15.82                                  | 2368       | 0.08                                       | 2368       | 25.53                                       | 2358       |
| -18.39                                  | 2378       | 0.06                                       | 2378       | -3.88                                       | 2368       |
| -4.44                                   | 2388       | -0.05                                      | 2388       | -33.15                                      | 2378       |
| 21.18                                   | 2398       | 0.2  | 2398       | 98.53                                       | 2388       |
| 49.9                                    | 2408       | 0.22                                       | 2408       | 130.67                                      | 2398       |
| 22.34                                   | 2418       | 0.29                                       | 2418       | 120.05                                      | 2408       |
| -1.47                                   | 2428       | 0.22                                       | 2428       | 72.57                                       | 2418       |
| 17.19                                   | 2438       | 0.03                                       | 2438       | 6.72  | 2428       |
| 15.21                                   | 2448       | 0.11                                       | 2448       | 55.93                                       | 2438       |
| -14.12                                  | 2458       | 0.16                                       | 2458       | 59.89                                       | 2448       |
| -24.15                                  | 2468       | -0.04                                      | 2468       | -31.79                                      | 2458       |
|   |            |  |            | -13.92                                      | 2468       |

SUBSTITUTE SHEET (RULE 26)

Table 6b. Components of possible prediction equations from multivariate regression analyses.

| Digestibility of dry matter <i>in vitro</i> |            |             | Digestibility of dry matter <i>in vivo</i> |             |            |
|---|------------|-------------|--|-------------|------------|
| PLS (2,5,6)                                 |            | PCR (2,5,6) | PLS (2,5,6)                                |             | Wavelength |
| Coefficient                                 | Wavelength | Coefficient | Wavelength                                 | Coefficient | Wavelength |
| 59.77                                       | 1108       | 40.58       | 1108                                       | 63.64       | 1108       |
| -98.28                                      | 1118       | -181.5      | 1118                                       | -78.7       | 1118       |
| 7.55  | 1128       | 12.91       | 1128                                       | 4           | 1128       |
| 12.25                                       | 1138       | 22.04       | 1138                                       | 8.88        | 1138       |
| 6.85  | 1148       | 19.61       | 1148                                       | 3.94        | 1148       |
| 6.74  | 1158       | 8.19        | 1158                                       | 7.06        | 1158       |
| 11.89                                       | 1168       | 5.29        | 1168                                       | 6.24        | 1168       |
| 4.45  | 1178       | -0.92       | 1178                                       | 0.43        | 1178       |
| -10.08                                      | 1188       | -11.1       | 1188                                       | -5.6        | 1188       |
| -28.8                                       | 1198       | -37.4       | 1198                                       | -15.1       | 1198       |
| -20.43                                      | 1208       | -28.13      | 1208                                       | -10.61      | 1208       |
| -20.05                                      | 1218       | -36.03      | 1218                                       | -15.98      | 1218       |
| -15.55                                      | 1228       | -35.84      | 1228                                       | -13.16      | 1228       |
| 2.41  | 1238       | -13.39      | 1238                                       | 2.93        | 1238       |
| 6.62  | 1248       | 0.89        | 1248                                       | 6.37        | 1248       |
| 8.6   | 1258       | 14.13       | 1258                                       | 7.08        | 1258       |
| 7.47  | 1268       | 17.48       | 1268                                       | 5.99        | 1268       |
| -1.32                                       | 1278       | -7.44       | 1278                                       | -0.25       | 1278       |
| -7.39                                       | 1288       | -22.67      | 1288                                       | -4.08       | 1288       |
| -0.79                                       | 1298       | -1.05       | 1298                                       | 0.15        | 1298       |
| 3.48  | 1308       | 9.23        | 1308                                       | 3.72        | 1308       |
| 5.1   | 1318       | 13.17       | 1318                                       | 4.38        | 1318       |
| 6.23  | 1328       | 15.6        | 1328                                       | 8.03        | 1328       |
| 8.48  | 1338       | 25.91       | 1338                                       | 9.03        | 1338       |
| 17.78                                       | 1348       | 40.71       | 1348                                       | 13          | 1348       |
| 24.61                                       | 1358       | 51.12       | 1358                                       | 13.51       | 1358       |
| -0.07                                       | 1368       | 4.6         | 1368                                       | 0.26        | 1368       |
| -23.89                                      | 1378       | -88.33      | 1378                                       | -13.81      | 1378       |
| -29.86                                      | 1388       | -68.78      | 1388                                       | -8.13       | 1388       |
| -16.97                                      | 1398       | 5.08        | 1398                                       | -1.4        | 1398       |
| 23.92                                       | 1408       | 32.14       | 1408                                       | 16.08       | 1408       |
| 60.7  | 1418       | 76.51       | 1418                                       | 32.08       | 1418       |
| 55.51                                       | 1428       | 80.84       | 1428                                       | 11.94       | 1428       |
| -0.3  |            | -1.47       |  | -14.76      |            |

Table 6b. Components of possible prediction equations from multivariate regression analyses.

| Digestibility of dry matter <i>in vitro</i> |            |  | Digestibility of dry matter <i>in vivo</i> |            |             |            |
|---|------------|--|--|------------|-------------|------------|
| PLS (2,6,6)                                 |            |  | PCR (2,6,6)                                |            | PLS (2,6,6) |            |
| Coefficient                                 | Wavelength |  | Coefficient                                | Wavelength | Coefficient | Wavelength |
| -28.21                                      | 1438       |  | -11.15                                     | 1438       | -19.94      | 1438       |
| -32.57                                      | 1448       |  | 10.5                                       | 1448       | -19.24      | 1448       |
| -28.08                                      | 1458       |  | 18.31                                      | 1458       | -16.15      | 1458       |
| 1.48  | 1468       |  | -3.92                                      | 1468       | 3.7         | 1468       |
| 18.21                                       | 1478       |  | -18.48                                     | 1478       | 10.65       | 1478       |
| -0.65                                       | 1488       |  | -25.14                                     | 1488       | -0.75       | 1488       |
| -22.99                                      | 1498       |  | -74.43                                     | 1498       | -7.65       | 1498       |
| -23.44                                      | 1508       |  | -75.49                                     | 1508       | -8.41       | 1508       |
| -15.74                                      | 1518       |  | -58.78                                     | 1518       | -8.08       | 1518       |
| -9.09                                       | 1528       |  | -25.77                                     | 1528       | -5.21       | 1528       |
| -2.8  | 1538       |  | -7.83                                      | 1538       | -3.83       | 1538       |
| 10.62                                       | 1548       |  | 17.83                                      | 1548       | 4.58        | 1548       |
| 28.78                                       | 1558       |  | 52.88                                      | 1558       | 15.5        | 1558       |
| 5.02  | 1568       |  | 21.09                                      | 1568       | 2.31        | 1568       |
| -8.6  | 1578       |  | -27.42                                     | 1578       | -3.09       | 1578       |
| -18.09                                      | 1588       |  | -42.59                                     | 1588       | -5.77       | 1588       |
| -9.28                                       | 1598       |  | -53.69                                     | 1598       | -8.48       | 1598       |
| -8.88                                       | 1608       |  | -3.08                                      | 1608       | -0.65       | 1608       |
| -3.82                                       | 1618       |  | -1.62                                      | 1618       | -0.87       | 1618       |
| -3.58                                       | 1628       |  | -2.81                                      | 1628       | 0.24        | 1628       |
| 0.65  | 1638       |  | -9.18                                      | 1638       | 3.42        | 1638       |
| 0.5   | 1648       |  | 13.81                                      | 1648       | 0.86        | 1648       |
| 23.87                                       | 1658       |  | 61.39                                      | 1658       | 13.12       | 1658       |
| 54.92                                       | 1668       |  | 159.8                                      | 1668       | 28.91       | 1668       |
| 78.84                                       | 1678       |  | 101.05                                     | 1678       | 44.01       | 1678       |
| -13.9                                       | 1688       |  | -79.36                                     | 1688       | -8.19       | 1688       |
| -74.54                                      | 1698       |  | -77.73                                     | 1698       | -34         | 1698       |
| -38.63                                      | 1708       |  | -43.87                                     | 1708       | -18.38      | 1708       |
| 24.48                                       | 1718       |  | 21.34                                      | 1718       | 2.17        | 1718       |
| -17.91                                      | 1728       |  | -25.8                                      | 1728       | -31.77      | 1728       |
| -43.01                                      | 1738       |  | -40.51                                     | 1738       | -21.21      | 1738       |
| -29.25                                      | 1748       |  | -28.11                                     | 1748       | -5.24       | 1748       |
| -16.33                                      | 1758       |  | -4.55                                      | 1758       | -11.87      | 1758       |
| 0.43  | 1768       |  | 2.68                                       | 1768       | -0.49       | 1768       |
| 28.21                                       | 1778       |  | 20.91                                      | 1778       | 21.37       | 1778       |
| 18.92                                       | 1788       |  | 13.59                                      | 1788       | 13.25       | 1788       |
| 0.54  | 1798       |  | 9.35                                       | 1798       | -0.93       | 1798       |



Table 6b. Components of possible prediction equations from multivariate regression analyses.

| Digestibility of dry matter <i>in vitro</i> |            |  | Digestibility of dry matter <i>in vivo</i> |            |             |            |
|---|------------|--|--|------------|-------------|------------|
| PLS (2,5,6)                                 |            |  | PCR (2,5,6)                                |            | PLS (2,5,6) |            |
| Coefficient                                 | Wavelength |  | Coefficient                                | Wavelength | Coefficient | Wavelength |
| -2.44                                       | 1808       |  | 7.17                                       | 1808       | -4.5        | 1808       |
| -2.72                                       | 1818       |  | -15.36                                     | 1818       | -2.3        | 1818       |
| -5.84                                       | 1828       |  | -29.4                                      | 1828       | -3.37       | 1828       |
| -4.37                                       | 1838       |  | -16.21                                     | 1838       | -0.05       | 1838       |
| -8.79                                       | 1848       |  | 2.3  | 1848       | -2.23       | 1848       |
| -7.72                                       | 1858       |  | -0.87                                      | 1858       | -3.78       | 1858       |
| -29.93                                      | 1868       |  | -21.29                                     | 1868       | -9.61       | 1868       |
| -98.16                                      | 1878       |  | -82.33                                     | 1878       | -34.56      | 1878       |
| -118.18                                     | 1888       |  | -102.15                                    | 1888       | -52.89      | 1888       |
| 117.59                                      | 1898       |  | 211.27                                     | 1898       | 38.2        | 1898       |
| 185   | 1908       |  | 204.51                                     | 1908       | 66.78       | 1908       |
| 33.91                                       | 1918       |  | -3.12                                      | 1918       | 28.1        | 1918       |
| -35.31                                      | 1928       |  | 18.14                                      | 1928       | -3.79       | 1928       |
| -44.59                                      | 1938       |  | 35.39                                      | 1938       | -19.45      | 1938       |
| -9.28                                       | 1948       |  | -8.24                                      | 1948       | -6.41       | 1948       |
| 35.73                                       | 1958       |  | -11.32                                     | 1958       | 15.95       | 1958       |
| 28.58                                       | 1968       |  | -37.15                                     | 1968       | 13.49       | 1968       |
| 10.68                                       | 1978       |  | -44.26                                     | 1978       | 2.03        | 1978       |
| 10.98                                       | 1988       |  | -61.81                                     | 1988       | 0.57        | 1988       |
| 65.12                                       | 1998       |  | -72.2                                      | 1998       | 31.07       | 1998       |
| 83.13                                       | 2008       |  | -63.31                                     | 2008       | 38.57       | 2008       |
| 7.23  | 2018       |  | 37.37                                      | 2018       | -1.21       | 2018       |
| 0.99  | 2028       |  | 183.21                                     | 2028       | -9.38       | 2028       |
| -10.85                                      | 2038       |  | 156.68                                     | 2038       | -14.51      | 2038       |
| -84.48                                      | 2048       |  | -2.09                                      | 2048       | -54.72      | 2048       |
| -122.91                                     | 2058       |  | -178.03                                    | 2058       | -68.29      | 2058       |
| -35.85                                      | 2068       |  | -104.9                                     | 2068       | -1.89       | 2068       |
| 34.94                                       | 2078       |  | -7.7                                       | 2078       | 37.55       | 2078       |
| 28.83                                       | 2088       |  | 62.28                                      | 2088       | 27.17       | 2088       |
| 18.03                                       | 2098       |  | 54.28                                      | 2098       | 18.01       | 2098       |
| 5.09  | 2108       |  | 14.14                                      | 2108       | 15.52       | 2108       |
| -9.58                                       | 2118       |  | -40.31                                     | 2118       | 7.88        | 2118       |
| 9.79  | 2128       |  | 2.34                                       | 2128       | 13.25       | 2128       |
| 23.04                                       | 2138       |  | 28.94                                      | 2138       | 16.49       | 2138       |
| -10.93                                      | 2148       |  | -31.58                                     | 2148       | -6.42       | 2148       |
| -16.87                                      | 2158       |  | 3.05                                       | 2158       | -9.12       | 2158       |
| -41.78                                      | 2168       |  | -68.48                                     | 2168       | -27.35      | 2168       |

Table 6b. Components of possible prediction equations from multivariate regression analyses.

| Digestibility of dry matter <i>in vitro</i> |            | Digestibility of dry matter <i>in vivo</i> |            |             |            |
|---|------------|--|------------|-------------|------------|
| PLS (2,5,6)                                 |            | PCR (2,5,6)                                |            | PLS (2,5,6) |            |
| Coefficient                                 | Wavelength | Coefficient                                | Wavelength | Coefficient | Wavelength |
| -48.69                                      | 2178       | -107.52                                    | 2178       | -32.58      | 2178       |
| -14.5                                       | 2188       | -54.54                                     | 2188       | -12.58      | 2188       |
| -0.14                                       | 2198       | -11.17                                     | 2198       | 4.5         | 2198       |
| -7.15                                       | 2208       | -2.14                                      | 2208       | 4.87        | 2208       |
| -48.95                                      | 2218       | -43.88                                     | 2218       | -30.89      | 2218       |
| -18.22                                      | 2228       | -0.01                                      | 2228       | -19.94      | 2228       |
| 88.33                                       | 2238       | 100.18                                     | 2238       | 14.88       | 2238       |
| -24.11                                      | 2248       | 53.32                                      | 2248       | -53.79      | 2248       |
| 55.99                                       | 2258       | 81.52                                      | 2258       | 18.98       | 2258       |
| 110.08                                      | 2268       | 46.93                                      | 2268       | 80.27       | 2268       |
| 52.18                                       | 2278       | -9.18                                      | 2278       | 63.98       | 2278       |
| -89.38                                      | 2288       | 25.1                                       | 2288       | -35.58      | 2288       |
| -109.89                                     | 2298       | -47.83                                     | 2298       | -77.98      | 2298       |
| -54.11                                      | 2308       | -23.3                                      | 2308       | -81.38      | 2308       |
| 17.83                                       | 2318       | -73.92                                     | 2318       | 22.34       | 2318       |
| 23.71                                       | 2328       | -23.74                                     | 2328       | 48.6        | 2328       |
| 62.19                                       | 2338       | 13.64                                      | 2338       | 37.79       | 2338       |
| -58.18                                      | 2348       | -21.87                                     | 2348       | -48.16      | 2348       |
| -21.28                                      | 2358       | -77.28                                     | 2358       | -7.88       | 2358       |
| 4.01  | 2368       | -88.75                                     | 2368       | 18.34       | 2368       |
| 32.53                                       | 2378       | 28.42                                      | 2378       | 17.8        | 2378       |
| 35.58                                       | 2388       | 68.01                                      | 2388       | 1.95        | 2388       |
| -21.25                                      | 2398       | 22.17                                      | 2398       | -27.54      | 2398       |
| -70.01                                      | 2408       | -28.88                                     | 2408       | -50.39      | 2408       |
| -18.88                                      | 2418       | 8.02                                       | 2418       | -18.09      | 2418       |
| 61.66                                       | 2428       | 75.99                                      | 2428       | 17.75       | 2428       |
| 14.94                                       | 2438       | 58.83                                      | 2438       | -3.68       | 2438       |
| -11.88                                      | 2448       | 8.48                                       | 2448       | -11.21      | 2448       |
| 5.35  | 2458       | -4.33                                      | 2458       | 3.97        | 2458       |
| 10.49                                       | 2468       | -33.25                                     | 2468       | 11.29       | 2468       |

Table 7. Descriptions of forages used in Table 8.

| Sample<br>In<br>Table 8 | Genus          | Species                                   | Variety            | Common name      | Part of<br>plant | Process undergone | Stage of maturity                | Regrowth               |
|-------------------------|----------------|---|--------------------|------------------|------------------|-------------------|----------------------------------|------------------------|
| 1                       | <i>Panicum</i> | <i>coloratum</i>                          | Kababula CPI 16798 | Makarikari grass | erial            | dried and chaffed | mild bloom (9 weeks' regrowth)   | mild bloom - regrowth  |
| 2                       | <i>Panicum</i> | <i>maximum</i>                            | Colonio            | Guinea grass     | erial            | dried and chaffed | vegetative regrowth (4 weeks')   | vegetative regrowth    |
| 3                       | <i>Panicum</i> | <i>coloratum</i>                          | Bambaisi           | Makarikari grass | erial            | dried and chaffed | mild bloom (1 month's regrowth)  | mild bloom - regrowth  |
| 4                       | <i>Panicum</i> | <i>maximum</i>                            | Hamil              | Guinea grass     | erial            | dried and chaffed | early bloom (1 month's regrowth) | early bloom - regrowth |
| 5                       | <i>Panicum</i> | <i>coloratum</i> var <i>Makarikenense</i> | Burnett            | Makarikari grass | erial            | dried and chaffed | mild bloom (9 weeks' regrowth)   | mild bloom - regrowth  |
| 6                       | <i>Panicum</i> | <i>maximum</i> var. <i>trichoglume</i>    | Petrie             | Green Panic      | erial            | dried and chaffed | mild bloom (4 weeks' regrowth)   | mild bloom - regrowth  |

Table 8. Examples of energy required to shear, digestibility of dry matter *in vivo*, forage consumption constraint (FCC), and voluntary feed consumption (VFC)

| Sample<br>In<br>Table 7 | Energy required to<br>shear,<br>predicted using NIR <sup>1</sup><br>(kJ/m <sup>2</sup> ) | Digestibility of dry<br>matter <i>in vivo</i> ,<br>predicted using NIR <sup>2</sup><br>(%) | Predicted FCC <sup>3</sup><br>(g OM/d/MBW) <sup>4</sup> | Predicted VFC <sup>5</sup><br>(g OM/d/MBW) | Actual VFC<br>(g OM/d/MBW) | Actual VFC<br>(g OM/d) |
|-------------------------|--|--|---|--|----------------------------|------------------------|
| 1                       | 20.51  | 51.29  | 88.85   | 32.52                                      | 30.77                      | 534                    |
| 2                       | 18.70  | 54.73  | 68.92   | 44.95                                      | 39.47                      | 888                    |
| 3                       | 13.75  | 58.69  | 51.49   | 58.51                                      | 48.79                      | 848                    |
| 4                       | 13.18  | 59.59  | 48.41   | 54.34                                      | 53.58                      | 931                    |
| 5                       | 17.52  | 55.18  | 71.21   | 39.74                                      | 43.68                      | 759                    |
| 6                       | 18.63  | 55.88  | 66.55   | 43.01                                      | 45.68                      | 793                    |

<sup>1</sup> Predicted using the calibration equation from stepwise regression analysis (Table 8a).<sup>2</sup> Predicted using the calibration equation from stepwise regression analysis (Table 8a).<sup>3</sup> Predicted using predicted energy required to shear, and the relationship between energy required to shear and FCC.<sup>4</sup> Calculated from predicted FCC and predicted digestibility of dry matter *in vivo*.<sup>5</sup> Abbreviations used: organic matter (OM), metabolic body weight (MBW) = BW<sup>0.75</sup>

THE CLAIMS of the invention are as follows:

1. A method for determining a biomechanical property of a feed, the method comprising the steps of:
  - (a)     subjecting the feed to infrared radiation to obtain spectral data;  
5             and
  - (b)     using the spectral data to determine the biomechanical property;whereby, the biomechanical property of the feed is determined on the basis of the bond energies of the chemical constituents of the feed.
2. A method according to claim 1 wherein the biomechanical property of the  
10     feed is determined directly from the spectral data.
3. A method according to claim 1 wherein the spectral data is used to determine another property of the feed and the other property is used to determine the biomechanical property on the basis of a correlation between the other property and the biomechanical property.
- 15   4. A method according to claim 3 wherein the other property is ADF content, NDF content or lignin content.
5. A method according to claim 1 or claim 2 wherein the spectral data is a reflectance spectrum over a predetermined range of wavelengths.
6. A method according to claim 5 wherein the predetermined range is  
20     approximately 700nm to 3000nm.
7. A method according to claim 5 wherein the predetermined range is approximately 1100nm to 2500nm.

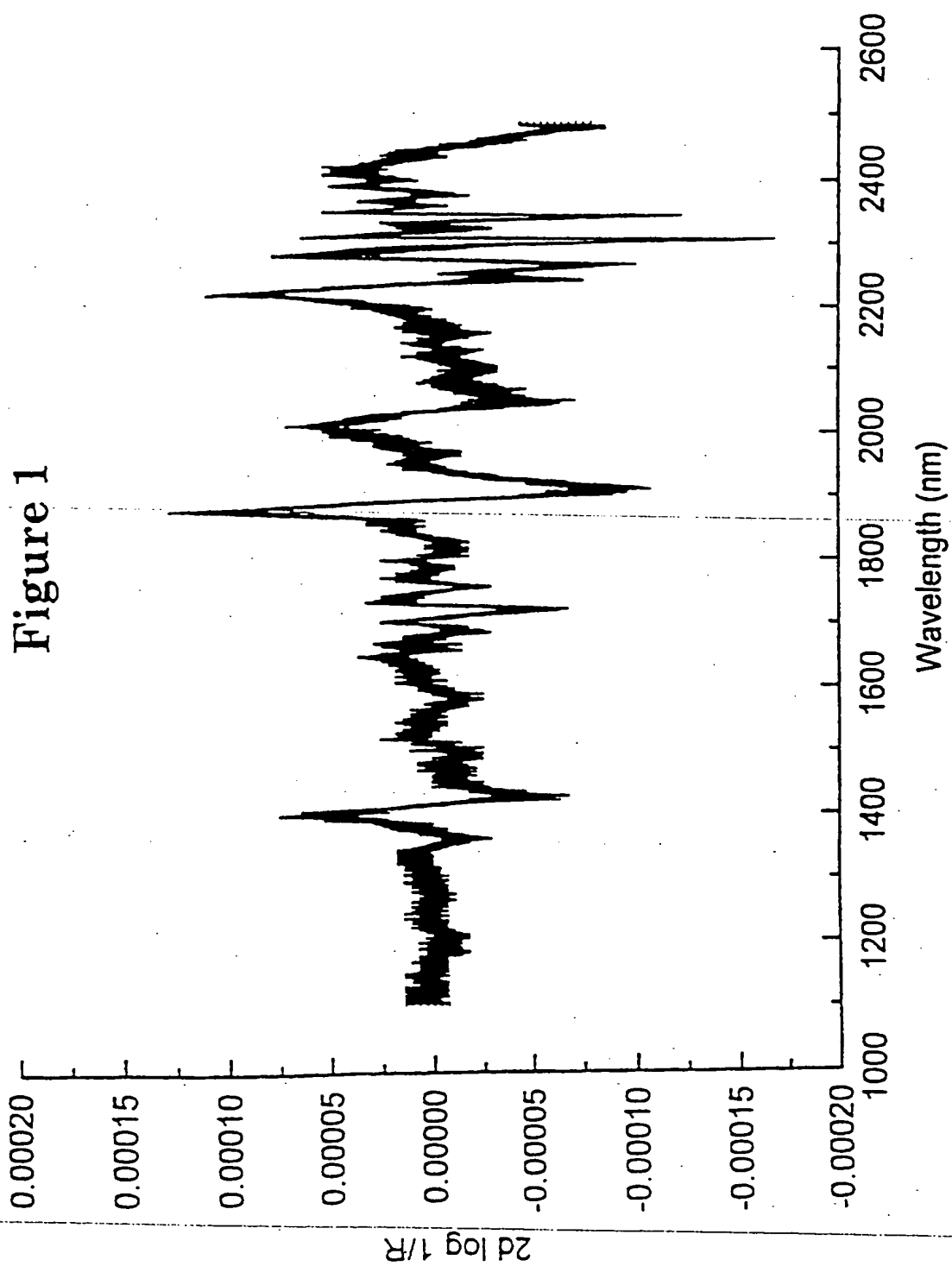
8. A method according to any one of claims 5 to 7 wherein the data obtained for the spectral range of approximately 1850nm to 1970nm is disregarded.
9. A method according to any one of claims 5 to 8 wherein the spectral data is recorded at 2nm intervals over the predetermined range.
- 5 10. A method according to claim 1 or claim 2 wherein the reflectance reading is taken at a combination of wavelengths.
11. A method according to claim 10 wherein the combination of wavelengths is selected from the group comprising: 1168nm, 1458nm, 1598nm, 1718nm, 1828nm, 2048nm, 1138nm, 2018nm, 2128nm, 2408nm, 1268nm, 1588nm,  
10 1728nm, 2278nm, 1158nm, 1238nm, 1668nm, 1908nm, 2248nm, 1698nm, 1748nm, 1918nm and 2158nm.
12. A method according to claim 10 wherein the combination of wavelengths is 1168nm, 1458nm, 1598nm, 1718nm, 1828nm and 2048nm and the biomechanical property is shear energy.
- 15 13. A method according to claim 10 wherein the combination of wavelengths is 1268nm, 1588nm, 1728nm and 2278nm and the biomechanical property is compression energy.
14. A method according to claim 10 wherein the combination of wavelengths is 1138nm, 2018nm, 2128nm and 2408nm and the biomechanical property is  
20 comminution energy.
15. A method for determining a biomechanical property of a feed, the method comprising the steps of:
  - (a) subjecting the feed to infrared radiation to obtain spectral data;  
and

- (b) comparing the spectral data obtained in (a) with a calibration equation to determine the biomechanical property;

whereby, the biomechanical property of the feed is determined on the basis of the bond energies of the chemical constituents of the feed.

- 5 16. A method according to claim 15 wherein the calibration equation is  $y_1 = 19.95 + 10239.46 R_{1168} + 3623.49 R_{1458} - 4255.61 R_{1598} - 5319.88 R_{1718} + 5148.38 R_{1828} + 2452.05 R_{2048}$  and the biomechanical property is shear energy( $y_1$ ).
- 10 17. A method according to claim 15 wherein the calibration equation is  $y_2 = 231.42 + 18224.74 R_{1138} - 4955.12 R_{2018} - 3005.37 R_{2128} + 4290.18 R_{2408}$  and the biomechanical property is comminution energy ( $y_2$ ).
18. A method according to claim 15 wherein the calibration equation is  $y_3 = -0.71 - 911.04 R_{1268} + 112.57 R_{1588} - 79.48 R_{1728} - 28.02 R_{2278}$  and the biomechanical property is compression energy ( $y_3$ ).
- 15 19. A method according to any one of claims 15 to 18 wherein the calibration equation is determined from laboratory data establishing a correlation between reflectance and the biomechanical property.
20. A method according to any one of claims 1 to 19 wherein an additional property of the feed is also determined.
- 20 21. A method according to claim 20 wherein the additional property of the feed is digestibility of dry matter *in vivo* or *in vitro*.
22. A method for determining feed quality, the method comprising the steps of:
- (a) subjecting the feed to infrared radiation to obtain spectral data;

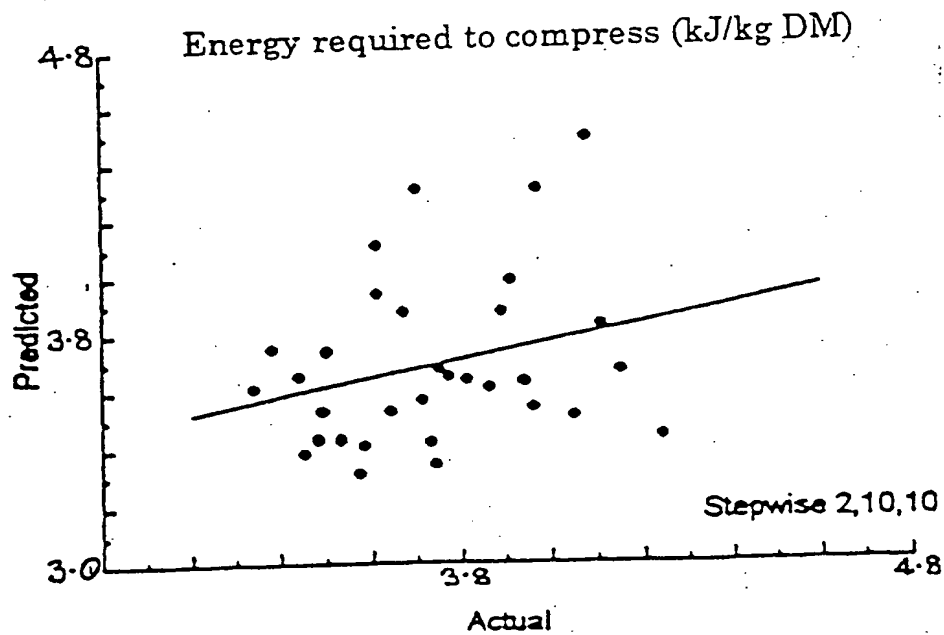
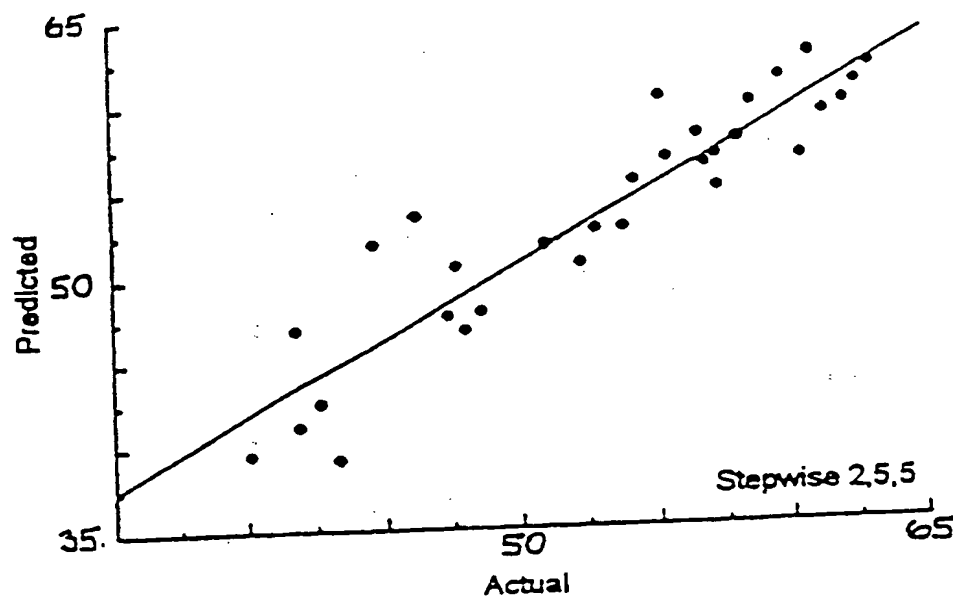
- (b) using the spectral data to determine a biomechanical property of the feed; and
  - (c) using the biomechanical property obtained in step (b) to determine feed quality;
- 5       whereby, the biomechanical property of the feed and thus feed quality is determined on the basis of the bond energies of the chemical constituents of the feed.
23. A method according to claim 22 wherein the feed quality is determined as a measure of voluntary feed consumption (VFC).
- 10   24. A method according to claim 22 wherein the feed quality is determined as a measure of forage consumption constraint (FCC).
25. A method substantially as herein described with reference to the description of the examples.
- 15   26. A spectrometer configured to carry out the method according to any one of claims 1 to 21 wherein the spectrometer is adapted to receive a sample of feed and determine a biomechanical property of the feed.
27. A spectrometer configured to carry out the method according to any one of claims 22 to 24 wherein the spectrometer is adapted to receive a sample of feed and determine the quality of the feed.
- 20   28. A spectrometer according to claim 26 or 27 further comprising a data processing means for determining the biomechanical property or the quality of the feed.





2/11

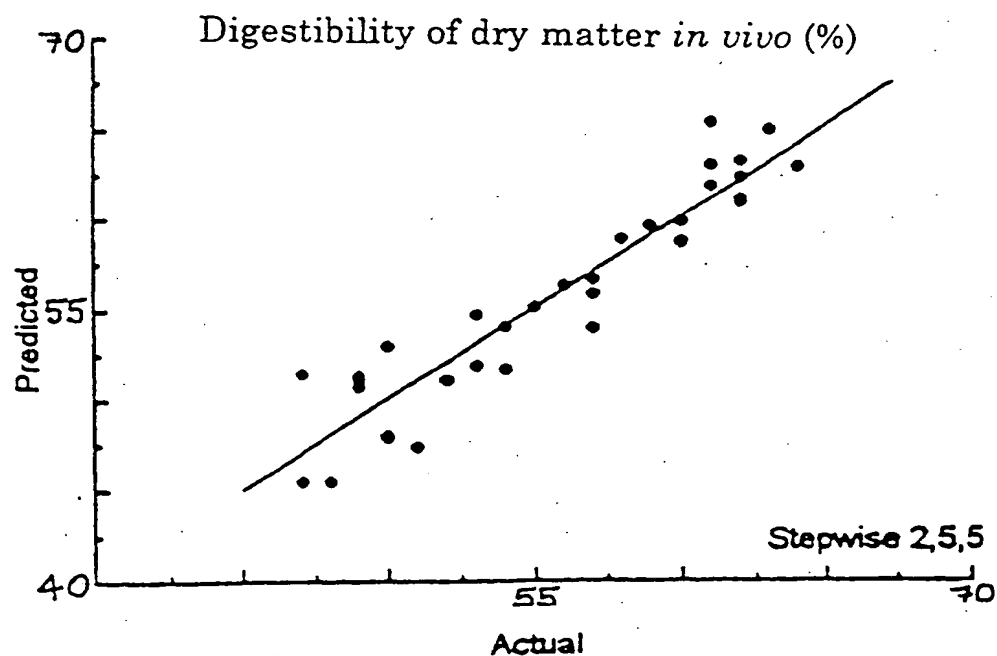
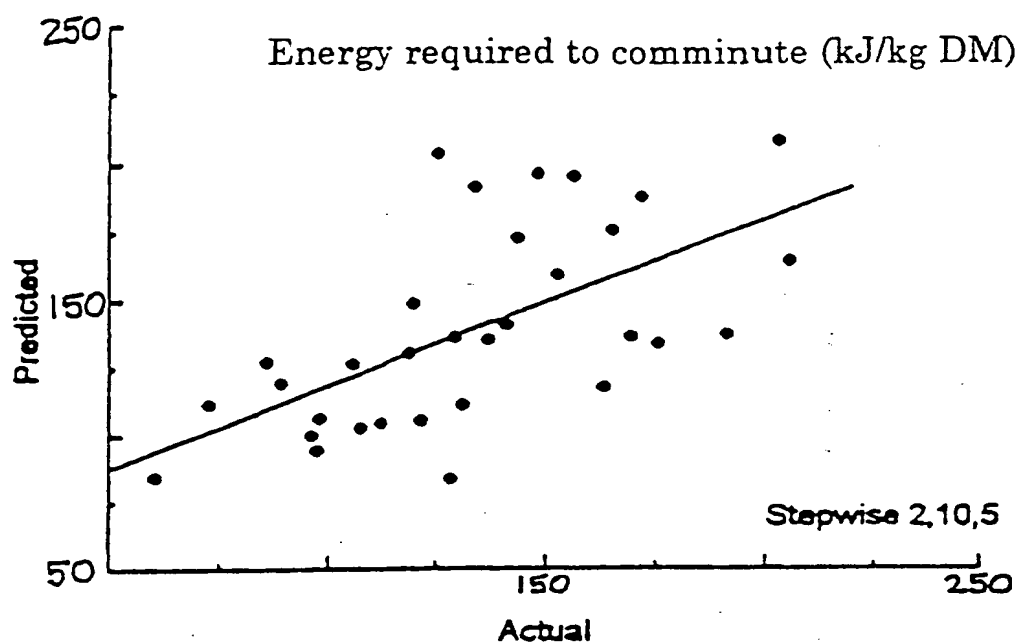
## Figure 2a

Digestibility of dry matter *in vitro* (%)

SUBSTITUTE SHEET (RULE 26)

3/11

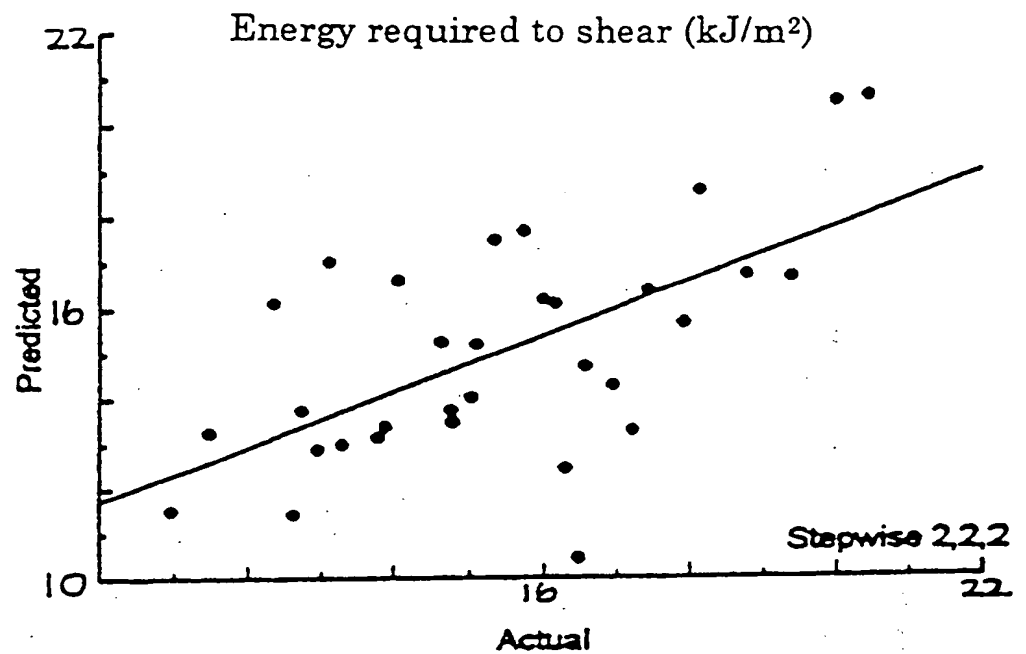
Figure 2a (cont'd)



SUBSTITUTE SHEET (RULE 26)

4/11

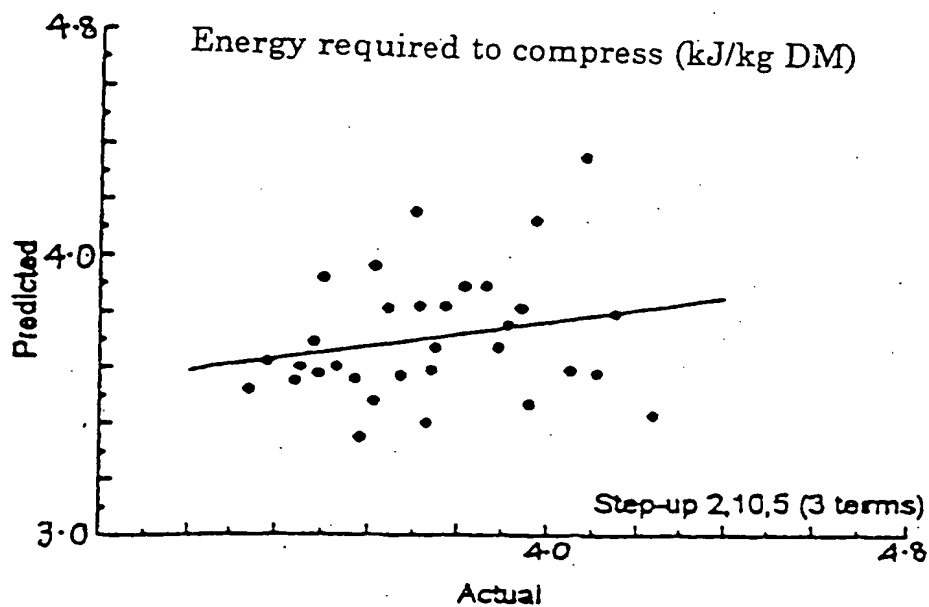
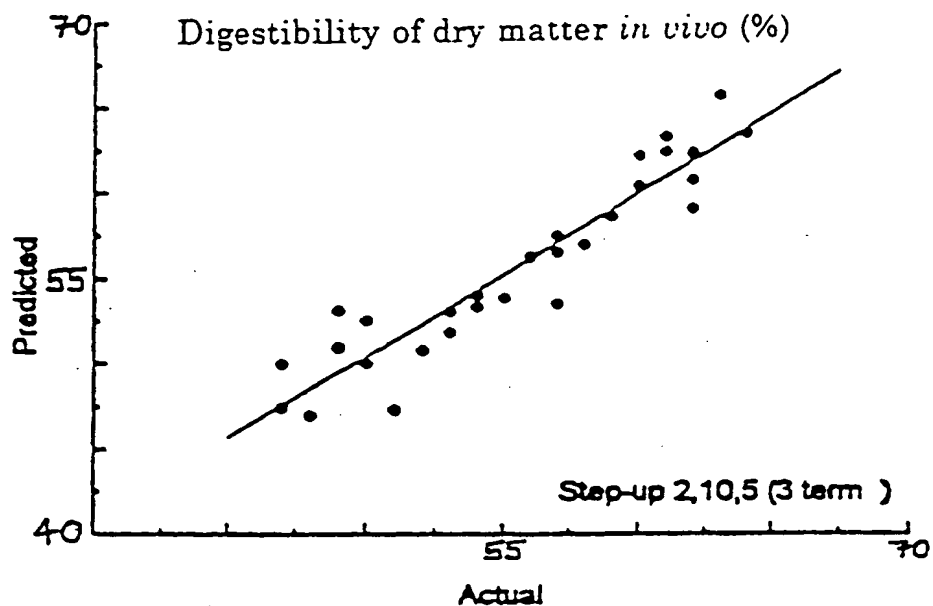
## Figure 2a (cont'd)



SUBSTITUTE SHEET (RULE 26)

5/11

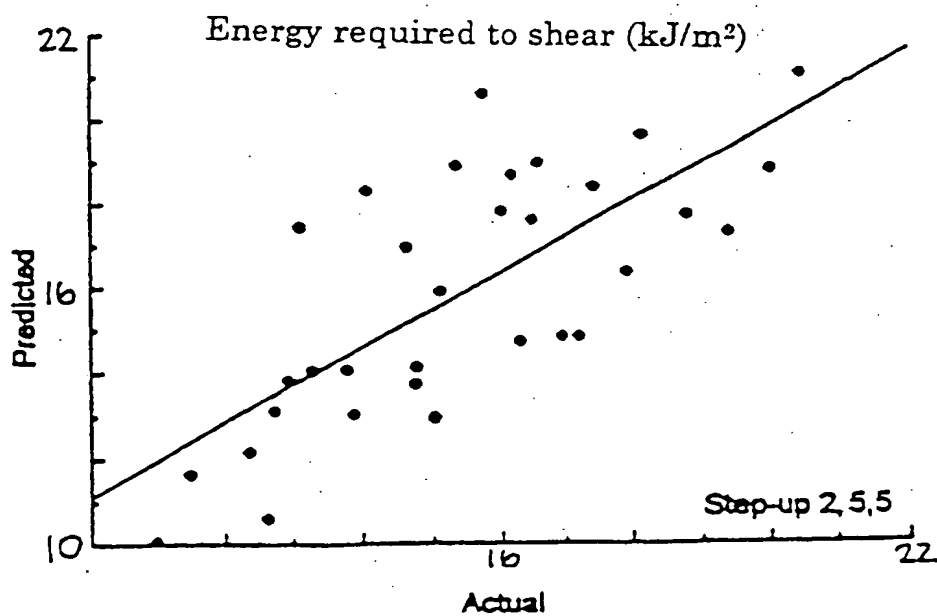
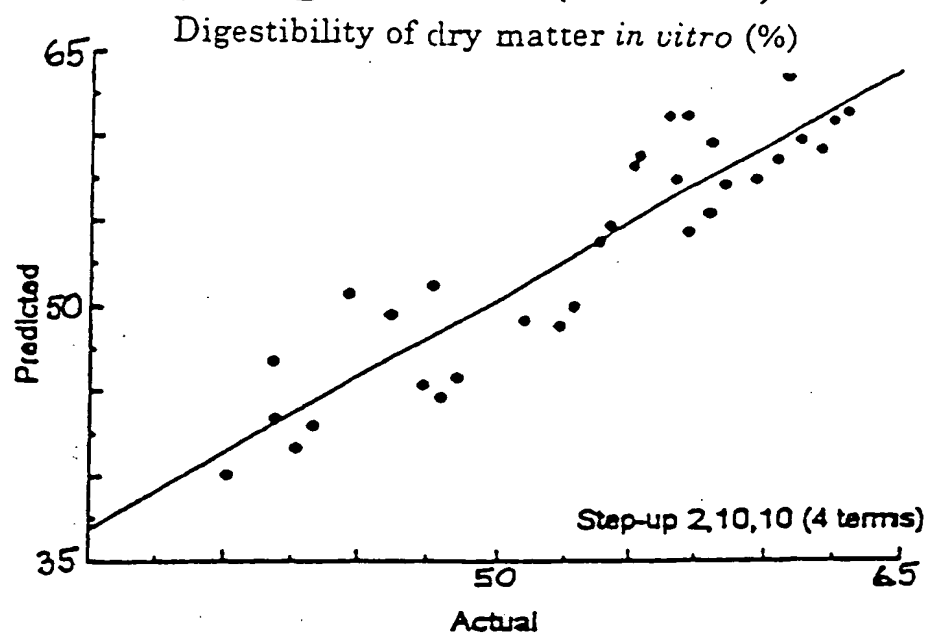
Figure 2b



SUBSTITUTE SHEET (RULE 26)

6/11

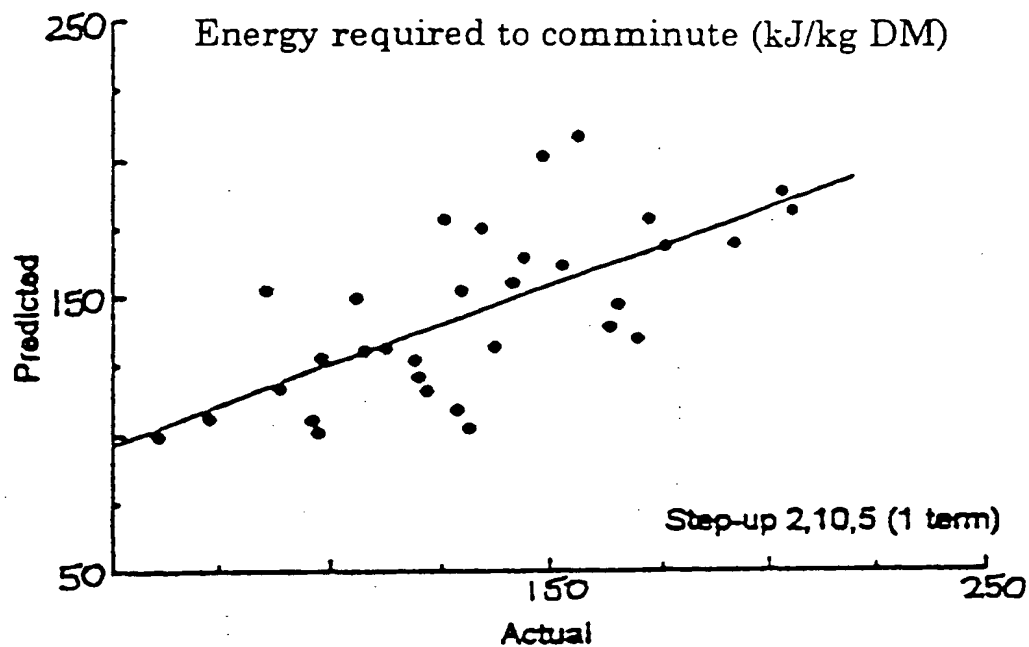
## Figure 2b (cont'd)



SUBSTITUTE SHEET (Rule 26)

7/11

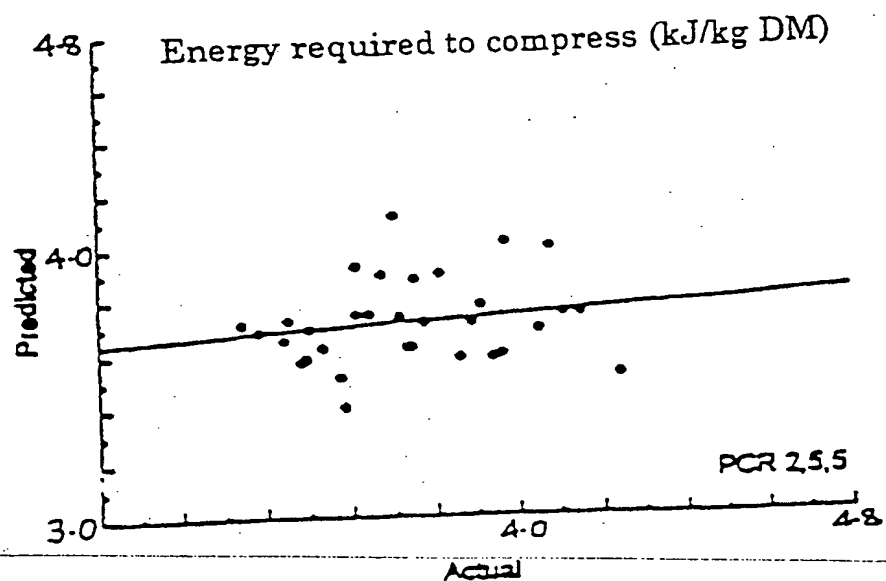
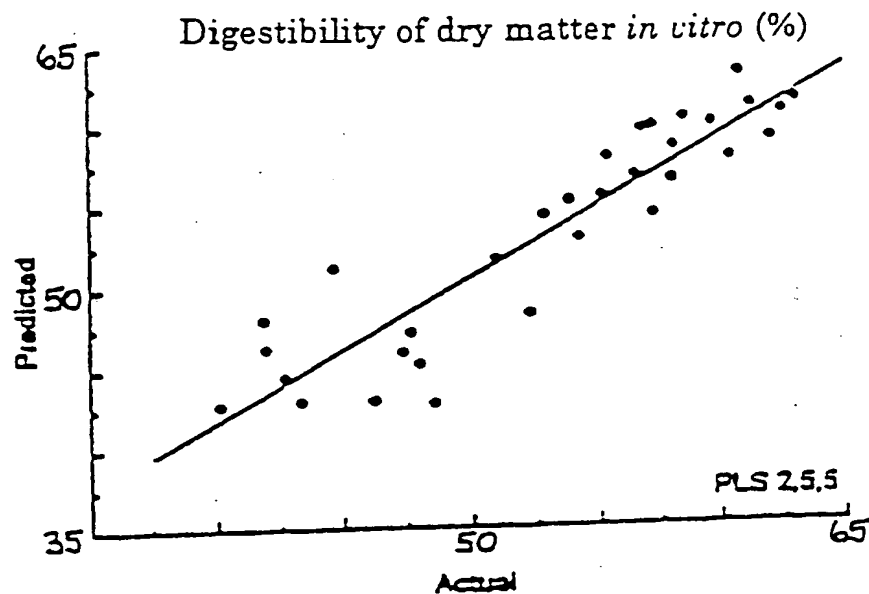
# Figure 2b (cont'd)



SUBSTITUTE SHEET (RULE 26)

8/11

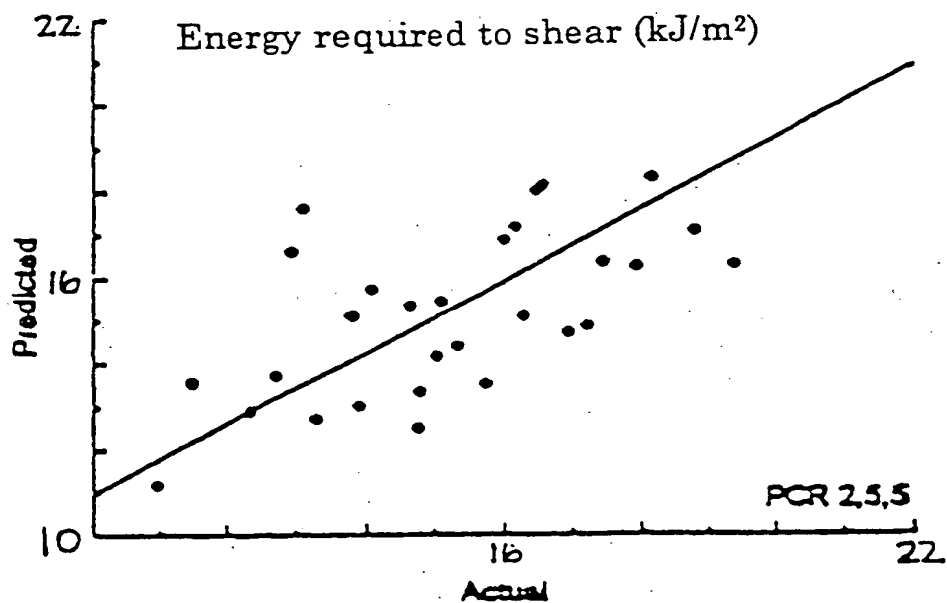
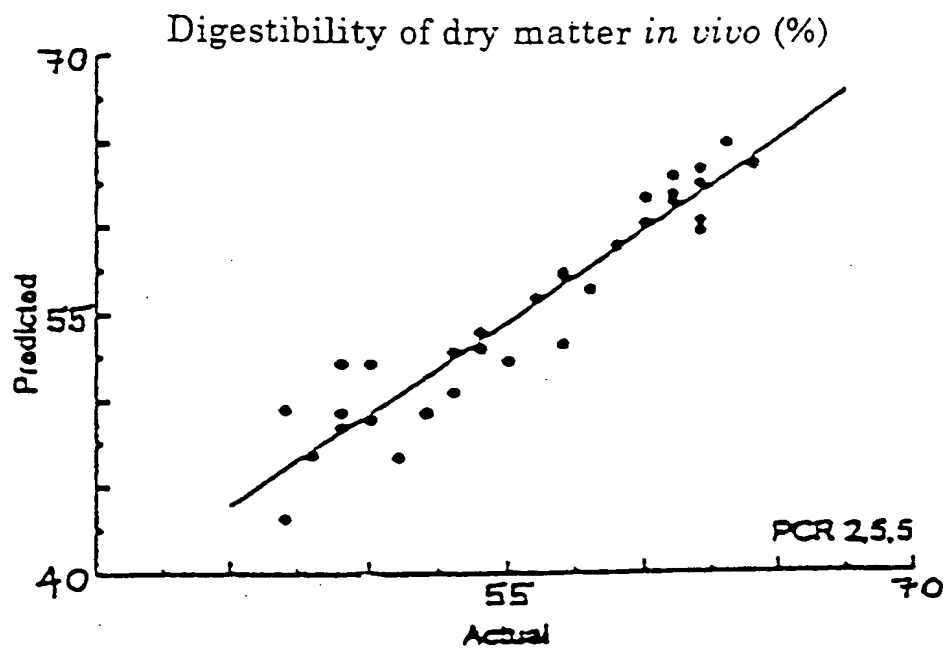
Figure 2c



SUBSTITUTE SHEET (RULE 26)

9/11

## Figure 2c (cont'd)

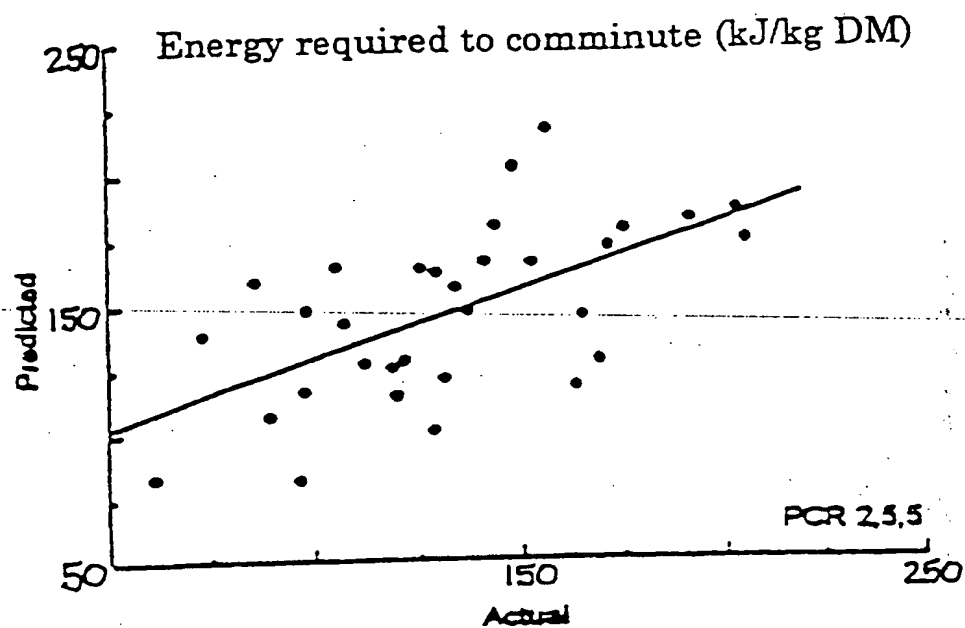


SUBSTITUTE SHEET (RULE 26)



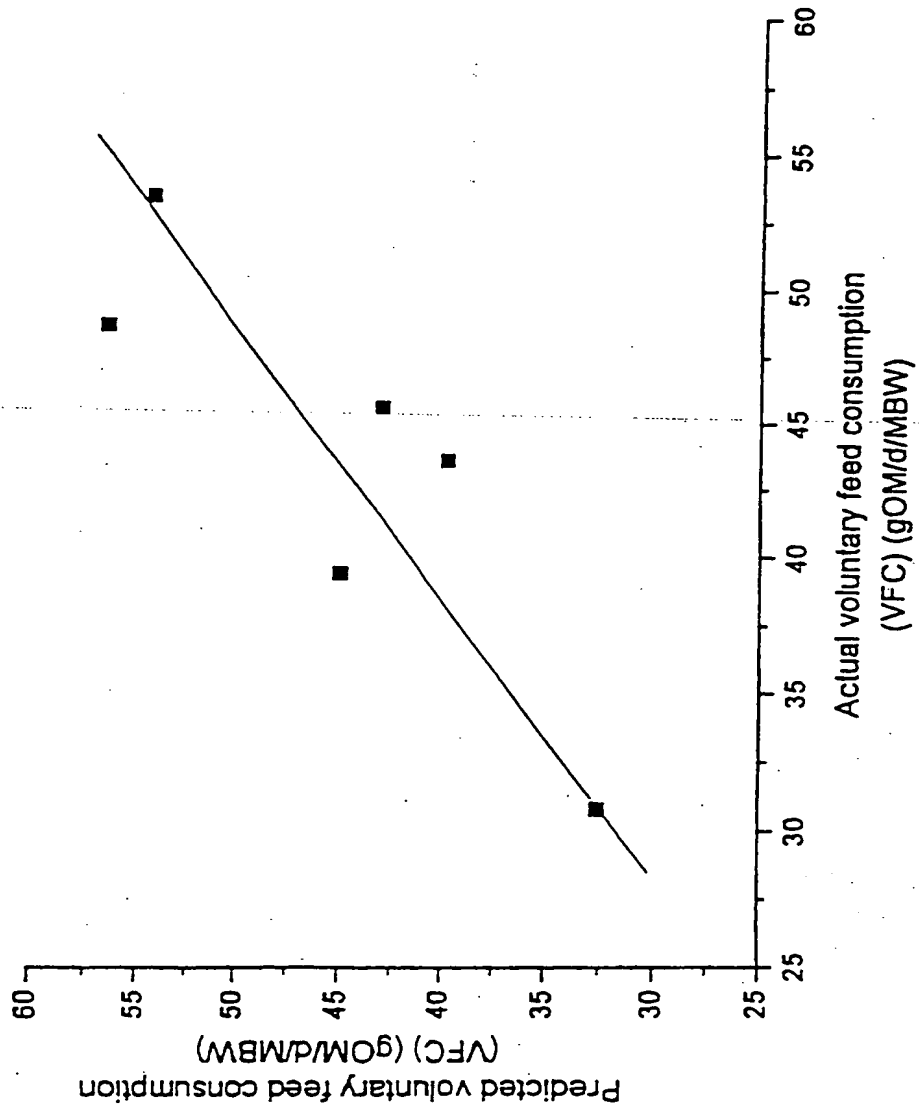
10/11

Figure 2c (cont'd)



SUBSTITUTE SHEET (RULE 26)

Figure 3



## INTERNATIONAL SEARCH REPORT

International Application No.  
PCT/AU 96/00776

| <b>A. CLASSIFICATION OF SUBJECT MATTER</b>   |   |   |
|--|---|---|
| Int Cl <sup>6</sup> : G01N 21/35, G01J 3/42  |   |   |
| According to International Patent Classification (IPC) or to both national classification and IPC  |   |   |
| <b>B. FIELDS SEARCHED</b>  |   |   |
| Minimum documentation searched (classification system followed by classification symbols)<br>IPC: G01N 21/34, 21/35, 33/02, G01J 3/28, 3/42  |   |   |
| Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched<br>AU:IPC as above   |   |   |
| Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)<br>WPAT, JAPIO: (IR or infrared or infra(red), (bond: or energ:)<br>DIALOG: "Science" Supergroup: [(IR or infrared or infra(red) and (bond? or energ?) and spectr? and (feed or fodder or hay)]   |   |   |
| <b>C. DOCUMENTS CONSIDERED TO BE RELEVANT</b>  |   |   |
| Category*  | Citation of document, with indication, where appropriate, of the relevant passages  | Relevant to claim No.   |
| X  | Animal Feed Science and Technology, Vol. 37 No. 3-4, 1992 Elsevier Science Publishers B.V., Amsterdam, "Influence of growth type and season on the prediction of the metabolisable energy content of herbage by near-infrared reflectance spectroscopy", pages 281-295 by D.I. GIVENS et al.<br>See entire document | 1-28  |
| X  | Animal Feed Science and Technology, Vol. 51, February 1995, Elsevier Science B.V., "The use of NIRS to predict the chemical composition and the energy value of compound feeds for cattle", pages 243-253 by J.L. de BOEUER et al.<br>See entire document   | 1-28  |
| <input checked="" type="checkbox"/> Further documents are listed in the continuation of Box C <input checked="" type="checkbox"/> See patent family annex  |   |   |
| <p>* Special categories of cited documents:</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"I" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&amp;" document member of the same patent family</p> |   |   |
| Date of the actual completion of the international search<br>26 February 1997  |   | Date of mailing of the international search report<br>06.03.97        |
| Name and mailing address of the ISA/VAU<br>AUSTRALIAN INDUSTRIAL PROPERTY ORGANISATION<br>PO BOX 200<br>WODEN ACT 2606<br>AUSTRALIA Facsimile No.: (06) 285 3929   |   | Authorized officer<br><br>GREG POWELL<br>Telephone No.: (06) 283 2308 |

## INTERNATIONAL SEARCH REPORT

International Application No.

PCT/AU 96/00776

## C (Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

| Category* | Citation of document, with indication, where appropriate, of the relevant passages  | Relevant to claim No. |
|-----------|---|-----------------------|
| X         | Proceedings 9th European Poultry Conference, Glasgow, UK, 7-12 August 1994: Volume 2. Symposia papers, published by WPSA, UK. "Current status of near infrared (NIR) spectroscopy in Australia for predicting metabolisable energy of poultry feeds", pages 106-109 by P.C. FLINN et al.<br>See entire document                               | 1-28                  |
| X         | Agri-Practice, Vol. 12, No. 3, May/June 1991, Veterinary Practice Pub. Co., USA, "Forage Analyses for Dietary Diagnosis and Management", pages 29-32 by B. ANDERSON et al.<br>See entire document   | 1-28                  |
| X         | Bulgarian Journal of Agricultural Science, Vol. 1, No. 1, 1995, Agricultural Academy of Bulgaria, "Estimation of Composition, Digestibility and Feeding Value of Forages by Near Infrared Reflectance Spectroscopy. II. Estimation of Energy Value and Protein Value of Forages" pages 35-44 by S.L. ATANASSOVA et al.<br>See entire document | 1-28                  |
| P,A       | WO 96/24843 A (WOLFKING DANMARK A/S) 15 August 1996<br>See page 9, lines 22-24<br>See page 11 line 18 - page 14 line 6<br>See page 16 line 28 - page 17 line 22<br>See page 18 line 13 - page 20 line 21<br>See Examples  | 1-28                  |
| A         | Derwent Abstract Accession No. 93-180660/22, Class S03, SU 1739284 A1 (UNIV DNEPR) 7 June 1992<br>See abstract  |                       |
| A         | Proceedings of the XVII International Grassland Congress 1993, "Genotypes of dry matured subterranean clover differ in shear energy", pages 592-593 by S.K. BAKER et al.<br>See entire document   |                       |
| A         | Proceedings of the XVII International Grassland congress 1993, "Composition of the fractions of dry mature subterranean clover digested <i>in vivo</i> and <i>in vitro</i> " pages 593-595 by L. KLEIN et al.<br>See entire document  |                       |
| A         | Patent Abstracts of Japan, E-78, page 1060, JP 53-15890 A (SHIMAZU SEISAKUSHO K.K.) 14 February 1978<br>See abstract  |                       |
| A         | Patent Abstracts of Japan, JP 06-123700 A (HAMAMATSU PHOTONICS KK) 6 May 1994<br>See abstract   |                       |
| A         | Patent Abstracts of Japan, P-393, page 58, JP 60-98335 A (KOGYO GIJUTSUIN (JAPAN)) 1 June 1985<br>See abstract  |                       |

# INTERNATIONAL SEARCH REPORT

## Information on patent family members

International Application No.  
PCT/AU 96/00776

This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

| Patent Document Cited in Search Report |         | Patent Family Member |             |    |             |    |             |
|--|---------|----------------------|-------------|----|-------------|----|-------------|
| WO                                     | 9624843 | AU                   | A1 46193/96 | AU | A1 46194/96 | AU | A1 46195/96 |
|  |         | DK                   | A 155/95    | DK | A 90/96     | DK | A 91/96     |

END OF ANNEX

